Abstract—The exact gain shape profile of erbium doped fiber amplifiers (EDFA's) are depends on fiber length and Er$^{3+}$ ion densities. This paper optimized several of erbium doped fiber parameters to obtain high performance characteristic at pump wavelengths of $\lambda_p=980$ nm and $\lambda_s=1550$ nm for three different pump powers. The maximum gain obtained for pump powers (10, 30 and 50mw) is nearly (19, 30 and 33 dB) at optimizations. The required numerical aperture NA to obtain maximum gain becomes less when pump power increased. The amplifier gain is increase when Er$^{3+}$doped near the center of the fiber core. The simulation has been done by using optisystem 5.0 software (CAD for Photonics, a license product of a Canadian based company) at 2.5 Gbps.

Keywords—EDFA, Erbium Doped Fiber, optimization Optical Amplifiers.

I. INTRODUCTION

ERBIUM doped fiber amplifiers (EDFA) play an important role in light wave communication systems. In order to transmit signals over long distances (>100 km), it is necessary to compensate for attenuation losses within the fiber because the cumulative effect of attenuation and dispersion make the signals to become weaker, indistinguishable and to be detected reliably [1]. Before this happens, the strength and shape of the signals must be restored. This can be done by using either a regenerator or an optical amplifier at an appropriate point along the length of the fiber. Electrical repeaters, which require optical-electrical signal conversion, have previously been used to compensate the power losses increasing with distance. The use of such repeaters in optical communication systems have made the systems more complex and increased their installation costs. The optical amplifiers enable the optical signals to be directly amplified optically. The fiber amplifiers can be made using different rare ions, the most interesting element is Erbium, because erbium doped fiber amplifiers (EDFA) made by doping the silica fiber with erbium ions can operate in a broad range within the 1550nm window at which the attenuation of silica fiber is minimum and therefore its ideal for the optical fiber communication systems operating at this wavelength range.

For maximum signal gain, first the fiber length must be chosen to some optimized value $L_{opt}$. This optimal length actually depends on the input pump power, since a longer length of inverted medium can be achieved by a higher pump. The optimum length also depends on both pump and signal wavelengths, since the pump absorption coefficient and the signal gain coefficient are wavelength dependent.

For saturated EDFAs, the optimum length also depends on the signal power [2]. The first part of the paper considers the optimization of fiber length relative to erbium ion density at three different pump powers assuming fundamental LP01 mode excitation at the pump wavelength ($\lambda_p=980$nm). The study shows that the optimum fiber length decreases when erbium ion densities increase.

The second part of the study considers the optimization of numerical aperture for optimum fiber length and erbium ion density at two different pump powers. The last part considers the effect of concentrating the Er$^{3+}$doping near the center of the fiber core on the signal gain.

II. THE CONFIGURATION OF EDFA

The main components of an EDFA should be at least consisting of:

1. The erbium-doped optical fiber
2. The pump laser
3. The wavelength-selective coupler.

The pump light is guided into the erbium-doped fiber by means of a wavelength division multiplexing (WDM), which is used to couple the pump signal into the doped fiber. Additionally, an isolator is generally placed at the output of an amplifier to prevent back reflection which can degrade amplifier performance or cripple the amplifier due to laser oscillation in the amplifier. Typically, the EDFA configuration can be categorized by pumping schemes into three particular arrangements. These schemes are:

1. Forward-pumped (co-pumped).
3. Dual-pumped.
Efficient EDFA pumping is possible using semiconductor lasers operating near 980- and 1480-nm wavelengths. The required pump power can be reduced by silica fibers doped with aluminum and phosphorus or by using fluorophosphates fibers with the availability of visible semiconductor lasers, EDFAs can also be pumped in the wavelength range 0.6-0.7µm. Most EDFA use 980-nm pump lasers as such lasers are commercially providing more than 100mw of pump power, and it’s used where low-noise is required. Pumping at 1480nm requires longer fibers and higher powers because it uses the tail of the absorption band, and it’s used for higher power amplifiers [3].

Pumping at a suitable wavelength provides gain through population inversion the gain spectrum depends on the pumping scheme as well as on the presence of other dopants, such as germanium and alumina, within the fiber core [3].

III. SIMULATION MODEL

Giles algorithm calculation was used which provides a full spectral solution and the propagation equation is integrated back and forth along the fiber in an iterative numerical process until the solution converges, or the maximum number of iterations is reached and additional loss mechanism such as pump excited state absorption ESA, and the effects of background loss are only considered during the Giles algorithm calculation. A simpler method of fiber characterization can be done by writing the amplifier equations in terms of Er3+ absorption coefficient (αk), gain coefficient (gk), and a fiber saturation parameter (ζ). These parameters can be obtained by conventional fiber measurement techniques.

The saturation parameter (ζ) can be defined theoretically as [4]:

\[ \zeta = \pi \cdot b_{eff}^2 \cdot n_i / \tau \]  

where \( b_{eff} \) is the equivalent radius of the doped region, \( n_i \) is local erbium ion density, and \( \tau \) is metastable life time parameter.

And the absorption and gain coefficients are expressed in terms of distributions of the ions and optical modes: [4]

\[ \alpha_k(\lambda_k) = \sigma_a(\lambda_k) \cdot \frac{2\pi e^2}{0} \int_{0}^{2\pi} i_k(r, \phi) \cdot n_i(r, \phi, z) r dr d\phi \]  

(2)

where \( i_k(r, \phi) \) is defined as the normalized optical intensity.

For a uniform ion distribution the absorption and gain coefficients can be simplified as [4]:

\[ \alpha_k(\lambda_k) = \Gamma(\lambda_k) \cdot \frac{n_i}{n_i} \cdot \sigma_a(\lambda_k) \]  

(4)

\[ g_k(\lambda_k) = \Gamma(\lambda_k) \cdot \frac{n_i}{n_i} \cdot \sigma_a(\lambda_k) \]  

(5)

Giles and Desurvire wrote the propagation equation in terms of saturation parameter, with absorption and emission coefficients:

\[ \frac{dp_k(z)}{dz} = u_k \cdot P_k(z) \left( \frac{g_k((v_i) + \alpha_k(v_i))}{n_i} - \alpha_k(v_i) - h_k \right) + u_k \cdot P_o \cdot g_k(v_k) \frac{n_i}{h_k} \]  

(6)

Where each beam propagates in the forward (\( u_k = 1 \)) or backward (\( u_k = -1 \)) direction and \( P_o \) means the spontaneous emission contribution from the local metastable population \( n_2 \);

\[ P_o = n_2 \cdot h \cdot v_k \Delta v_k \]  

Where \( h \) is normalized number of modes, and \( \Delta v_k \) is the noise band width, and \( l_k \) is the background loss.

In the same way, the steady-state solution of rate equation may be written as: [4]

\[ \frac{n_i}{n_i}(z) = \frac{\sum_{k=1}^{N} P_k(z) \cdot \alpha_k(v_k) \cdot h \cdot v_k \cdot n_i}{1 + \sum_{k=1}^{N} P_k(z) \cdot (\alpha_k(v_k) + g_k(v_k))} \]  

(7)

The above two equations (6) and (7) are referenced further as a Giles model. These equations are solved in the homogeneous line broadening case.

IV. EDFA SIMULATION PROGRAM

After entering the required parameters for a desired amplifier in main menu and sub menus of the program, the optimization can be made for the EDFA’s. The main menu and some of the simulation program are shown in Fig. 2.
V. TYPICAL EDFA CHARACTERISTIC OBTAINED WITH SIMULATION PROGRAM

Table I shows the typical EDFA parameters used in the simulation program.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Value</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>Pump absorption cross section</td>
<td>( \sigma_{pa} )</td>
<td>( 1.8 \times 10^{-25} ) m²</td>
<td></td>
</tr>
<tr>
<td>signal absorption cross section</td>
<td>( \sigma_{sa} )</td>
<td>( 2.14 \times 10^{-25} ) m²</td>
<td></td>
</tr>
<tr>
<td>Pump emission cross section</td>
<td>( \sigma_{se} )</td>
<td>( 3.15 \times 10^{-25} ) m²</td>
<td></td>
</tr>
<tr>
<td>signal input power</td>
<td>( P_s )</td>
<td>-30 dBm</td>
<td></td>
</tr>
<tr>
<td>Signal wavelength</td>
<td>( \lambda_s )</td>
<td>980 nm</td>
<td></td>
</tr>
<tr>
<td>Pump wavelength</td>
<td>( \lambda_p )</td>
<td>1550 nm</td>
<td></td>
</tr>
</tbody>
</table>

A. Optimization of Length at Different Erbium Ion Densities

The optimization was done at three different pump powers (10, 30 and 50mw) for the fiber length equal to 50m and Erbium ion density swept from (1 to 1000 ppm-wt). Figs. 4 and 5 show the value of gain according to the Er\(^{3+}\) ion density relative to optimum fiber length. According to the result at optimization EDFA can be designed by inserting optimum length with the value of erbium ion density in which gain is maximum at each of three different pump powers.

It is shown that when Erbium ion density increases the optimum length decreases which is suitable for lumped amplifier, but we must take into account, that in practical applications, the value of Erbium ion density = 1000 ppm-wt which correspond to \((1 \times 10^{25} \text{ m}^{-3})\) considered as an upper limit for the Erbium ion density in EDFAs, because high concentration of Er\(^{3+}\) deleterious gain due to clustering, this effect is known as cooperative energy transfer (CET) which reduces fluorescence lifetime.

It is seen from Fig. 5 that for 10mw pumping power the gain is low due to insufficient population inversion.

B. Change of Numerical Aperture (NA) at Optimum Fiber Length

Optimum fiber length with its relative Er\(^{3+}\) ion density at each of pumping powers (30 and 50 mw) is chooses. From Fig. 3 at 30mw, for optimum length (10.8m) the erbium ion density equal to(526 ppm), and at pump power 50mw for the same density the optimum length is equal to (12.2m) which chooses. The NA is swept from (0.1 to 0.3).

The other parameters are the same as mentioned before. Fig. 6 shows the signal gain as function of numerical aperture. It is seen that the gain increases with increasing NA and remains constant (saturate) after certain level for each pump power, the reason for this is that the amplifier reaches the population inversion. It is clear that the gain increases when NA increases because increasing NA proves the overlap between optical mode field and erbium ions. Also with increasing pump power the required NA to obtain maximum gain becomes less.
The erbium doping radius was ranged from (1 to 15 μm), and fiber core radius equal to 2.2 μm. Fig. 7 shows the signal gain as function of Er³⁺-doped radius (r₀). The Er³⁺ ion density was assumed to be 526ppm-wt. The pump wavelength is 980nm and the pump power is 30 and 50 mw. The signal wavelength is 1550nm and the signal power is -30dBm. The signal gain increases as doping radius decreases, because the signal light does not suffer from additional absorption. That is, the Er³⁺- ions does not exist in the area where the pump power is small. It is shown that concentrating the erbium doping near the fiber –axis results, at low pump power, in improvement maximum gain, because the inner region of the core is inverted and has gain the outer region that is not inverted is absorbing.

VI. CONCLUSION

1) The optimum fiber length decreases when erbium ion densities increase. According to the result, it is possible to design amplifiers with high gain for amplifier length as short as few meters by increasing erbium ion density and vise versa. The maximum gain obtained for pump powers (10, 30 and 50mw) is nearly (19, 30 and 33 dB) at optimizations.

2) The required numerical aperture NA to obtain maximum gain becomes less when pump power increased.

3) The maximum gain is obtained when erbium doping radius is less than the fiber core radius and concentrating the erbium doping near the fiber –axis results, at low pump power, in improvement maximum gain. The optimum erbium doped radius for the two different pump powers (30 and 50mw) are 1.96 and 2.06μm respectively.

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REFERENCES


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