

Analysis of Conduction-Radiation Heat Transfer in a Planar Medium: Application of the Lattice Boltzmann Method

Ahmed Mahmoudi, Imen Mejri, Mohamed A. Abbassi, Ahmed Omri

Abstract—In this paper, the 1-D conduction-radiation problem is solved by the lattice Boltzmann method. The effects of various parameters such as the scattering albedo, the conduction-radiation parameter and the wall emissivity are studied. In order to check on the accuracy of the numerical technique employed for the solution of the considered problem, the present numerical code was validated with the published study. The found results are in good agreement with those published

Keywords—Conduction, lattice Boltzmann method, planar medium, radiation.

I. INTRODUCTION

NUMERICAL modeling of the coupled transient radiative conductive heat transfer is an important field of research because of its relevance in various engineering applications such as the measurement of thermo-physical properties and the thermal control by ceramics and low density refractory material, heat transfer through the semitransparent, porous materials, multilayered insulations, glass fabrication, industrial furnaces, optical textile fiber processing, fibrous insulation [1]-[5]. In recent years, use of the lattice Boltzmann method (LBM) as a potential computational fluid dynamics (CFD) tool for the solution of a large class of problems in science and engineering [6]-[9] has gained a momentum. As a different approach from the conventional CFD solvers, the LBM uses simple microscopic kinetic models to simulate complex transport phenomena. Its advantages include, among others, simple calculation procedure, simple and efficient implementation for parallel computation, easy and robust handling of complex geometries, and high computational performance with regard to stability and accuracy. With the successful applications of the LBM to a large class of fluid mechanics problems, Ho et al. [10], [11] solved a non-Fourier heat conduction problem in a planar medium using the LBM. Solidification of a planar medium using the LBM was analyzed by Jiaung et al. [12]. Srinivasan et al. [13] analyzed microscale heat transfer in multilayered thin films using parallel computation of the Boltzmann transport equation. Guo

and Zhao [14] solved a natural-convection problem and used temperature-dependent viscosity in the LBM formulation. Jamia et al. [15] used the LBM to solve natural-convection in a partitioned enclosure with inclined partitions attached to its hot wall. Chatterjee et al. [16] used the LBM to analyze solid-liquid phase transitions in the presence of thermal diffusion. Quite recently, its application has also been extended to solve energy equations of conduction, convection, and radiation heat transfer problems. Raj et al. [17] used the LBM to analyze the solidification of a semitransparent planer layer; they used the discrete transfer method (DTM) to compute the radiative information. Mishra et al. [18] used the LBM to solve conduction-radiation problems in 1-D and 2-D rectangular geometries and used the finite volume method (FVM). Mondal et al. [19] used the lattice boltzmann method and the discrete ordinates method (DOM) for solving transient conduction and radiation heat transfer problems, they found that the LBM-DOM combination is in excellent agreement with the FDM-DOM combination, also The LBM-DOM was slightly faster than the FDM-DOM. Chaabane et al. [20] solved the conduction-radiation problems in enclosure using the lattice Boltzmann method and the control volume finite element method (CVFEM). Talukdar et al. [21] studied conduction-radiation problem using the collapsed dimension method (CDM) in one dimensional gray planar absorbing, emitting and anisotropically scattering medium. Mishra et al. [22] studied the performance of the collapsed dimension method (CDM) and the discrete transfer method (DTM) in terms of computational time and their abilities to provide accurate results in solving radiation and/or conduction mode problems in a 2-D rectangular enclosure. The CDM was found to be much more economical than the DTM.

In this paper, the 1-D conduction-radiation problem is solved by the lattice Boltzmann method. The effects of various parameters such as the scattering albedo, the conduction-radiation parameter, and the wall emissivity are studied. In order to check on the accuracy of the numerical technique employed for the solution of the considered problem, the present numerical code was validated with the published study.

II. MATHEMATICAL FORMULATION

A. Problem Statement

A one-dimensional planar medium of length L is considered for the present study. The initial condition at time $t = 0$ for the

Ahmed Mahmoudi is with Unité de Recherche Matériaux, Energie et Energies Renouvelables (MEER), Faculté des Sciences de Gafsa, B.P.19, Zarroug, Gafsa, 2112, Tunisie (Corresponding author; e-mail: ahmed.mahmoudi@yahoo.fr).

Imen Mejri, Mohamed A. Abbassi, and Ahmed Omri are with Unité de Recherche Matériaux, Energie et Energies Renouvelables (MEER), Faculté des Sciences de Gafsa, B.P.19, Zarroug, Gafsa, 2112, Tunisie (e-mail: im.mejri85@yahoo.fr, abbassima@gmail.com, ahom206@yahoo.fr).

temperature field $T(x,t)$ is given by $T(x,0) = T_E$ and the boundary conditions at $t > 0$ by $T(0, t) = T_E$ and $T(L, t) = T_w > T_E$. The west and the east boundaries are diffuse gray with emissivities ϵ_w and ϵ_E , respectively. β , ω , and N are the extinction coefficient, the scattering albedo, and the conduction-radiation parameter, respectively. For a homogeneous medium, the energy equation is given by:

$$\rho c_p \frac{\partial T}{\partial t} = k \nabla^2 T - \vec{\nabla} \cdot \vec{q}_R \quad (1)$$

where ρ is the density, c_p is the specific heat and k is the thermal conductivity. \vec{q}_R is the radiative heat flux.

B. Energy Equation

For a one-dimensional planar geometry, in the LBM with a D1Q2 lattice, the discrete Boltzmann equation with Bhatnagar-Gross-Krook (BGK) approximation is given by [9]:

$$\frac{\partial f_i(\vec{x}, t)}{\partial t} + \vec{e}_i \cdot \nabla f_i(\vec{x}, t) = -\frac{1}{\tau} [f_i(\vec{x}, t) - f_i^{eq}(\vec{x}, t)] \quad i = 1 \text{ and } 2 \quad (2)$$

where f_i is the particle distribution function denoting the number of particles at the lattice node \vec{x} and time t moving in direction i with velocity \vec{e}_i along the lattice $\Delta x = \vec{e}_i \Delta t$ connecting the neighbors, τ is the relaxation time, and f_i^{eq} is the equilibrium distribution function. The relaxation time τ for the D1Q2 lattice is computed from:

$$\tau = \frac{\alpha}{|\vec{e}_i|^2} + \frac{\Delta t}{2} \quad (3)$$

where α is the thermal diffusivity. For this lattice, the two velocities e_1 and e_2 , and their corresponding weights w_1 and w_2 , are given by:

$$e_1 = \frac{\Delta x}{\Delta t} \quad e_2 = -\frac{\Delta x}{\Delta t} \quad (4)$$

$$w_1 = w_2 = \frac{1}{2} \quad (5)$$

After discretization, (2) is written as:

$$f_i(\vec{x} + \vec{e}_i \Delta t, t + \Delta t) = f_i(\vec{x}, t) - \frac{1}{\tau} [f_i(\vec{x}, t) - f_i^{eq}(\vec{x}, t)] \quad (6)$$

The temperature is obtained after summing f_i over all direction:

$$T(\vec{x}, t) = \sum_{i=1,2} f_i(\vec{x}, t) \quad (7)$$

To process (6), an equilibrium distribution function is required, which for a conduction-radiation problem is given by:

$$f_i^{eq}(\vec{x}, t) = w_i T(\vec{x}, t) \quad (8)$$

To account for the volumetric radiation, the energy equation in the LBM formulation, (6) is modified to:

$$f_i(\vec{x} + \vec{e}_i \Delta t, t + \Delta t) = f_i(\vec{x}, t) - \frac{1}{\tau} [f_i(\vec{x}, t) - f_i^{eq}(\vec{x}, t)] - \frac{\Delta t w_i}{\rho c_p} \frac{\partial q_R}{\partial x} \quad (9)$$

where the divergence of radiative heat flux $\frac{\partial q_R}{\partial x}$ is given by:

$$\frac{\partial q_R}{\partial x} = \beta(1-\omega)(4\pi \frac{\sigma T^4}{\pi} - G) \quad (10)$$

G is the incident radiation.

C. Radiative Information

In the problem under consideration, the energy transport in any direction \vec{s} is exclusively governed by the radiative transfer equation:

$$\frac{1}{c} \frac{\partial I(\vec{x}, \vec{s}, t)}{\partial t} + \frac{\partial I(\vec{x}, \vec{s}, t)}{\partial s} = -\beta I(\vec{x}, \vec{s}, t) + \beta(1-\omega)I_b(\vec{x}, t) + \frac{\beta\omega}{4\pi} \int_{\Omega=4\pi} I(\vec{x}, \vec{s}', t) p(\vec{s}' \rightarrow \vec{s}) d\Omega' \quad (11)$$

where c is the speed of light in the medium, S is the energy transport direction, $I_b = \sigma T^4 / \pi$ is the Planck's black body intensity, $d\Omega$ is the solid angle and $p(s' \rightarrow s)$ the anisotropic scattering phase function. Equation (11) can be recast as:

$$\frac{1}{c} \frac{\partial I(\vec{x}, \vec{s}, t)}{\partial t} + \vec{s} \cdot \nabla I(\vec{x}, \vec{s}, t) = -\beta I(\vec{x}, \vec{s}, t) + \beta S(\vec{x}, \vec{s}, t) \quad (12)$$

where S is the radiative source term given as:

$$S(\vec{x}, \vec{s}, t) = (1-\omega)I_b(\vec{x}, t) + \frac{\omega}{4\pi} \int_{\Omega=4\pi} I(\vec{x}, \vec{s}', t) p(\vec{s}' \rightarrow \vec{s}) d\Omega' \quad (13)$$

The radiative boundary condition for (11), when the wall bounding the physical domain is assumed grey and emits and reflects diffusely, can be expressed as:

$$I(\vec{x}_E, \vec{s}) = \varepsilon_E I_b(\vec{x}_E) + \frac{(1-\varepsilon_E)}{\pi} \int_{\Omega=2\pi} [I(\vec{x}_E, \vec{s}) | \vec{n} \cdot \vec{s}]_{\vec{n} \cdot \vec{s} > 0} d\Omega' \quad (14)$$

$$I(\vec{x}_W, \vec{s}) = \varepsilon_W I_b(\vec{x}_W) + \frac{(1-\varepsilon_W)}{\pi} \int_{\Omega=2\pi} [I(\vec{x}_W, \vec{s}) | \vec{n} \cdot \vec{s}]_{\vec{n} \cdot \vec{s} < 0} d\Omega' \quad (15)$$

If anisotropic scattering is approximated by the linear anisotropic phase function $p = 1 + a \cos \gamma \cos \gamma'$, where a is the anisotropy factor ($-1 < a < 1$), (13) for the source term can be written as :

$$S(\vec{x}, \vec{s}, t) = (1-\omega)I_b(\vec{x}, t) + \frac{\omega}{4\pi} \int_{\Omega=4\pi} I(\vec{x}, \vec{s}, t)(1 + a \cos \gamma \cos \gamma') d\Omega' \quad (16)$$

$$S(\vec{x}, \vec{s}, t) = (1-\omega)I_b(\vec{x}, t) + \frac{\omega}{4\pi} [G(\vec{x}, t) + a \cos \gamma q_R(\vec{x}, t)] \quad (17)$$

γ is the polar angle.

Multiplying (12) throughout by the speed of light c , the radiative transfer equation along any lattice link designated by the index i can be written as:

$$\frac{DI_i}{Dt}(\vec{x}, \vec{s}, t) = \frac{\partial I_i}{\partial t} + \vec{c} \cdot \nabla I_i = -c\beta(I_i - S_i) \quad i=1, \dots, M \quad (18)$$

Let \vec{e}_i be the velocity of propagation along the i th lattice link of the DIQM lattice structure. If the velocity of light \vec{c} is fictitiously made equal to the velocity of particle propagation in the LBM, $\vec{c} = \vec{e}$ a convenient tool would be obtained to solve the radiative transfer equation using the LBM approach

$$\frac{\partial I_i}{\partial t} + \vec{e}_i \cdot \nabla I_i = e_i \beta (S_i - I_i) \quad i=1, \dots, M \quad (19)$$

Discretizing (19), we obtain:

$$I_i(\vec{x} + \vec{e}_i \Delta t, t + \Delta t) = I_i(\vec{x}, t) + \Delta t e_i \beta (S_i - I_i) \quad i=1, \dots, M \quad (20)$$

Clearly in (20), the term on the right hand side can be seen as the collision term in the LBM, where I_i is the intensity particle distribution function. Using the standard LBM terminology, (11) can be written as:

$$I_i(\vec{x} + \vec{e}_i \Delta t, t + \Delta t) = I_i(\vec{x}, t) + \frac{\Delta t}{\tau_R} [I_i^{eq}(\vec{x}, t) - I_i(\vec{x}, t)] \quad (21)$$

where τ_R is the relaxation time for the collision process and

I_i^{eq} is the equilibrium particle distribution function.

$$\tau_R = \frac{1}{e_i \beta} \quad \text{and} \quad I_i^{eq} = S_i \quad (22)$$

In (17), G is the irradiation and \vec{q}_R is the heat flux due to diffuse radiation, are computed from the following:

$$G = 4\pi \sum_{i=1, M} I_i \sin \gamma_i \sin \left(\frac{\Delta \gamma_i}{2} \right) \quad (23)$$

$$q_R = 2\pi \sum_{i=1, M} I_i \sin \gamma_i \cos \gamma_i \sin(\Delta \gamma_i) \quad (24)$$

III. RESULTS AND DISCUSSION

In this paper, the energy equation of a 1-D transient conduction- radiation problem is solved with LBM. Initially the medium is at temperature T_E . For $t > 0$, the west boundary temperature is maintained at $T_W = 2T_E$. The medium is absorbing, emitting and isotropically scattering. The non dimensional time step $\Delta \xi = 10^{-4}$ ($\xi = \alpha \beta^2 t$) was considered and steady state condition was assumed to have been achieved when the maximum variation in temperature at any location between two consecutive time levels did not exceed 10^{-5} . First the effect of the grid size to the non-dimensional temperature results (T/T_W) is studied by comparing the steady state (SS) results at three locations in the medium for several grid sizes for $\beta=1.0$, $N=0.1$, $T_E=0.0$, $T_W=1.0$, $\omega=0.5$ and $\varepsilon_w = \varepsilon_E = 1.0$. The results are listed in Table I and show that the non-dimensional temperature is stable and practically independent of the grid size.

TABLE I
 EFFECT OF GRID SIZE ON NON-DIMENSIONAL TEMPERATURE STEADY STATE
 FOR $\beta=1.0$, $T_E=0.0$, $T_W=1.0$, $\omega=0.5$, $N=0.1$ AND $\varepsilon_w=\varepsilon_E=1.0$

		$x/L = 0.25$	$x/L = 0.50$	$x/L = 0.75$
N_x=20	M=4	0.8265	0.6076	0.3339
	M=8	0.8356	0.6204	0.3438
	M=16	0.8389	0.6254	0.3479
	M=32	0.8400	0.6270	0.3492
M=32	N _x =20	0.8400	0.6270	0.3492
	N _x =30	0.8438	0.6210	0.3365
	N _x =40	0.8269	0.6181	0.3441
	N _x =60	0.8227	0.6152	0.3425

In Table II, for $\zeta = 0.05$ $\beta=1.0$, $N=0.1$, $T_E=0.0$, $T_W=1.0$, $\omega=0.5$, $\varepsilon_w = 1.0$ and $\varepsilon_E = 1.0$ or 0.0 , the non-dimensional temperature results (T/T_W) are compared with those reported in the literature [23], [24] at three locations in the medium, It is observed that the LBM results are in good agreements with the published results.

TABLE II
 COMPARISON OF TRANSIENT TEMPERATURE T/T_w AT TIME $\xi=0.05$ FOR $\beta=1.0$,
 $T_E=0.0$, $T_w=1.0$, $\omega=0.5$, $N=0.1$ AND TWO SETS OF WALL REFLECTIVITIES

		$x/L = 0.25$	$x/L = 0.5$	$x/L = 0.75$
$\epsilon_w = 1.0$	[23]	0.4888	0.1778	0.0591
	[24]	0.4889	0.1773	0.0588
$\epsilon_E = 1.0$	Present	0.4893	0.1787	0.05724
$\epsilon_w = 1.0$	[23]	0.5030	0.2005	0.0833
	[24]	0.5031	0.2001	0.0830
$\epsilon_E = 0.0$	present	0.5037	0.1993	0.0841

Figs. 1 (a)-(c) show the effect of the conduction-radiation parameter ($N=0.01, 0.1$ and 1.0) by comparing the LBM results (T/T_w) and those published [19] at different non dimensional time values for $\beta=1.0, \omega=0.0$ and $\epsilon_w = \epsilon_E = 1.0$. It is observed that the LBM results are in good agreements with those published.

Figs. 2 (a)-(c) show the effect of the scattering albedo ($\omega=0.1, 0.5$ and 0.9) by comparing the LBM results (T/T_w) and those published [19] at different non dimensional time values for $\beta=1.0, N=0.01$ and $\epsilon_w = \epsilon_E = 1.0$. Excellent agreement is found.

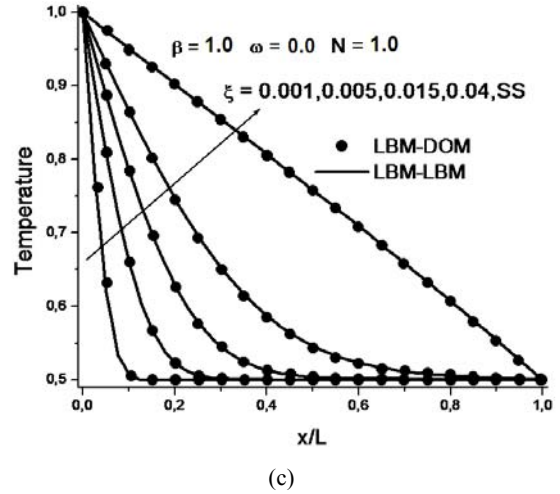
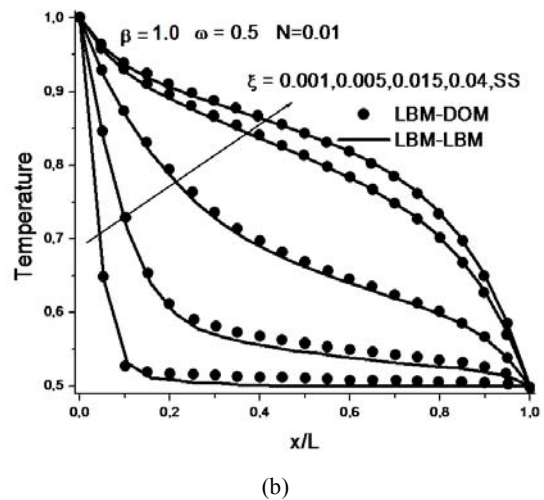
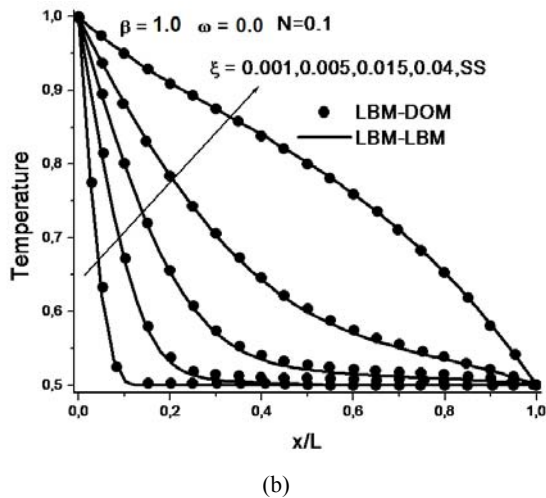
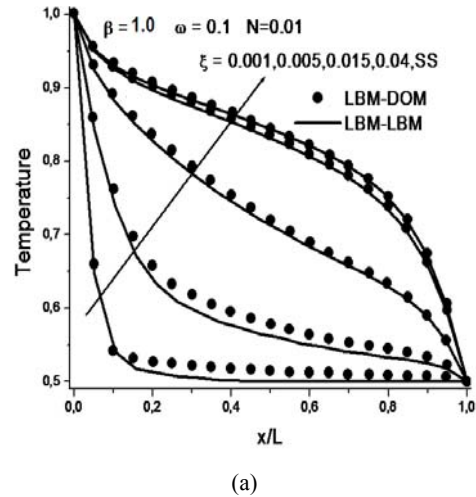
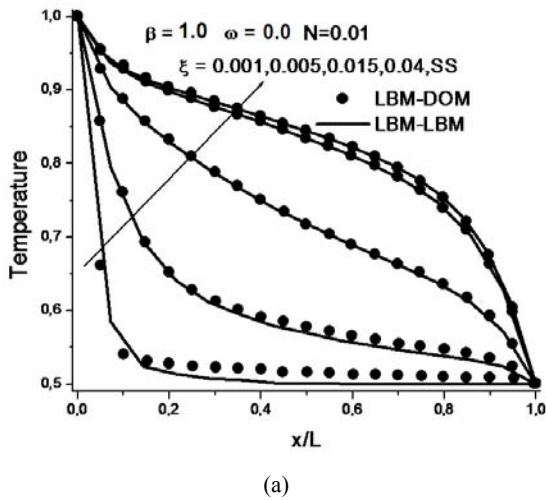
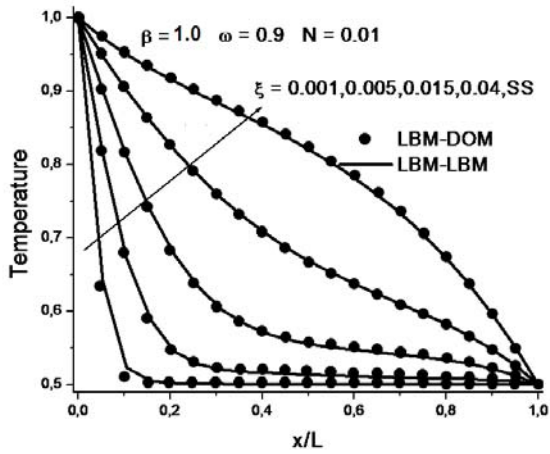
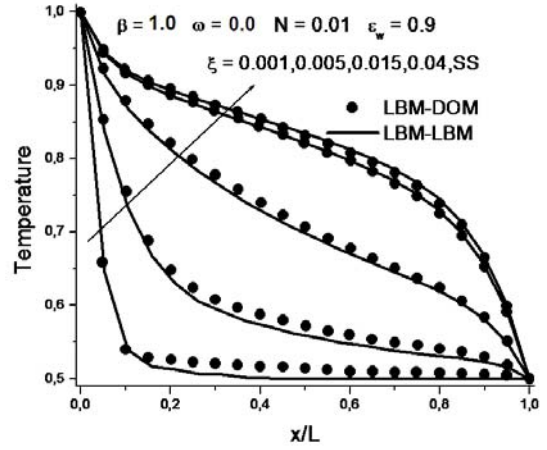


Fig. 1 Comparison of non-dimensional temperature (T/T_w) at different instants ξ for several conduction-radiation parameter (a) $N = 0.01$, (b) $N = 0.1$ and (c) $N = 1.0$.





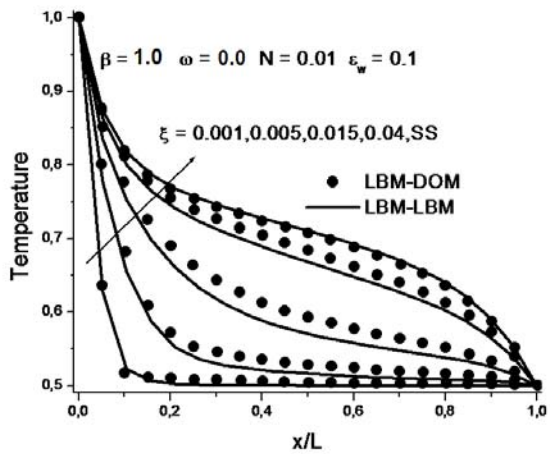
(c)



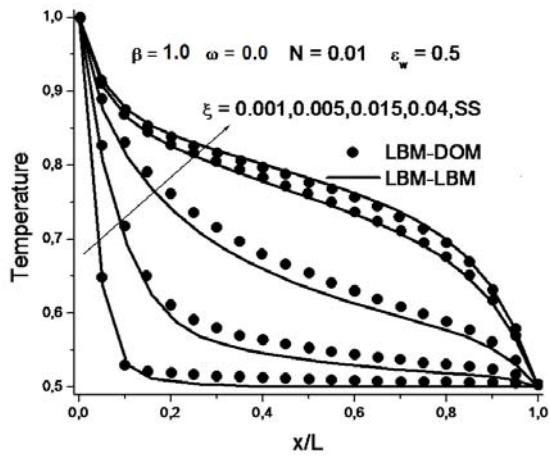
(c)

Fig. 2 Comparison of non-dimensional temperature (T/T_w) at different instants ξ for several scattering albedo (a) $\omega=0.1$ (b) $\omega=0.5$ and (c) $\omega=0.9$

Fig. 3 Comparison of non-dimensional temperature (T/T_w) at different instants ξ for several west boundary emissivity (a) $\epsilon_w = 0.1$ (b) $\epsilon_w = 0.5$ and (c) $\epsilon_w = 0.9$



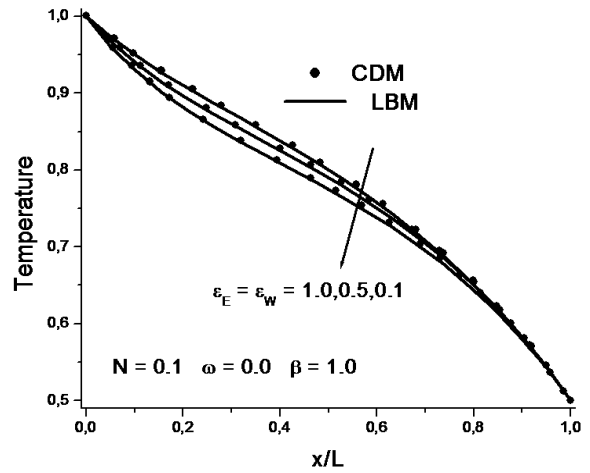
(a)



(b)

Figs. 3 (a)-(c) show the effect of the west boundary emissivity ($\epsilon_w = 0.1, 0.5$ and 0.9) by comparing the LBM results (T/T_w) and those published [19] at different non dimensional time values for $\beta=1.0, \omega=0.0, N=0.01$ and $\epsilon_E = 1.0$. Excellent agreement is also found.

Figs. 4 (a) and (b) show the effect of the emissivity by comparing the steady-state LBM results (T/T_w) and those published [21] for $\beta=1.0, \omega=0.0$ and respectively for $N=0.1$ and 0.01 . It is shown that the LBM results are in good agreements with those published.



(a)

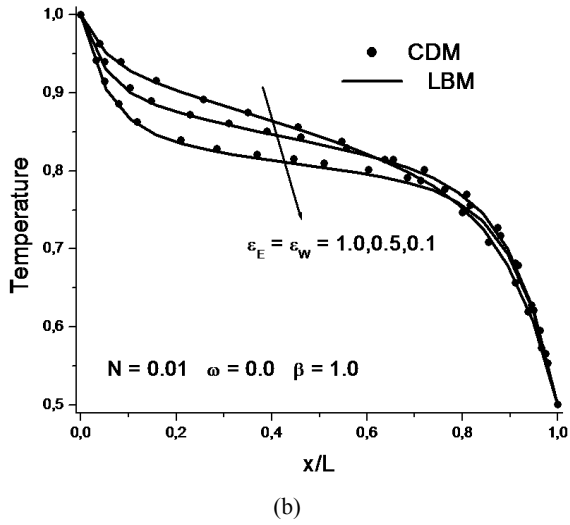


Fig. 4 Comparison of steady-state results (T/T_w) for $\beta=1.0$, $\omega=0.0$ (a) $N=0.1$ (b) $N=0.01$

Fig. 5 shows the effect of scattering albedo on temperature distribution. Both boundaries are assumed black. Three different values of scattering albedo ($\omega=0.0, 0.5$ and 1.0) are considered. The LBM results (T/T_w) are given for two sets of boundary temperatures ($T_E=0.1$ and 0.5) for $N=0.1$ and $\beta=1.0$. The LBM results are compared with those of [21]. Excellent agreement is found.

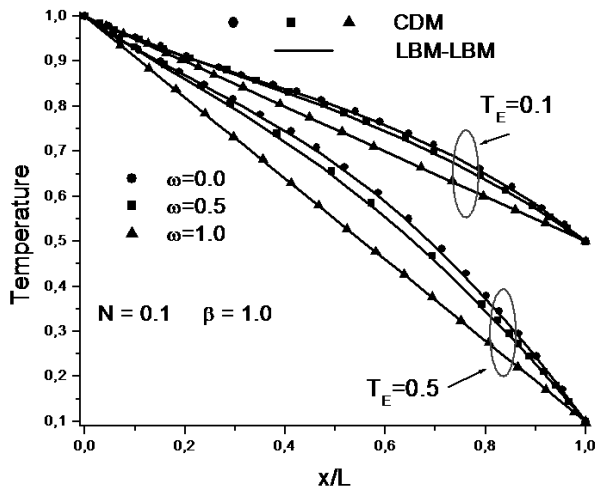


Fig. 5 Comparison of steady-state results (T/T_w) for several scattering albedo

Fig. 6 shows the effect of the extinction coefficient ($\beta=0.1, 1.0$ and 2.0) on temperature distribution. Both boundaries are assumed black. The LBM results (T/T_w) are given for $N=0.1$ and $\omega=0.0$. The LBM results are compared with those of [22]. Excellent agreement is found.

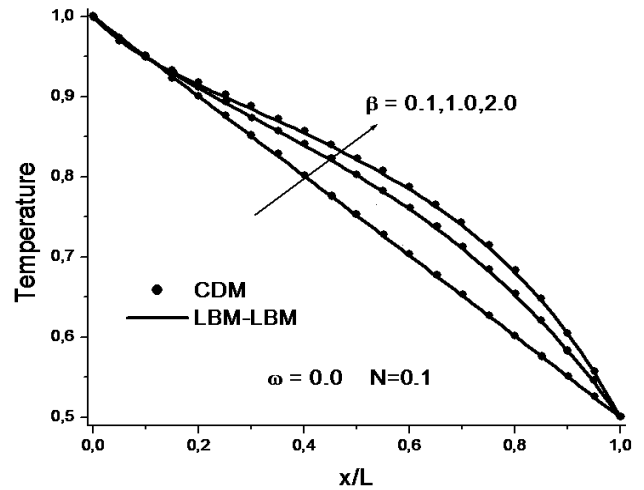
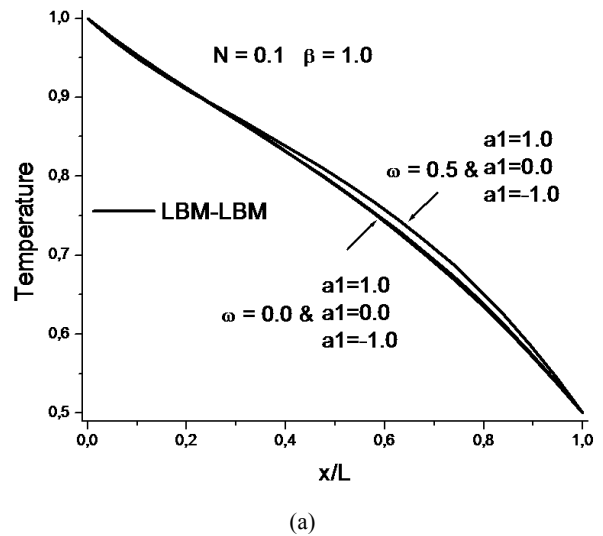


Fig. 6 Comparison of steady-state results (T/T_w) for several extinction coefficients

Figs. 7 (a) and (b) show the effect of the anisotropy factor a on non dimensional temperature distribution, for $N=0.1$, for two values of the scattering albedo $\omega=0.0$ and 0.5 and for two values of the extinction coefficient $\beta=0.1$ and 1.0 . Results are presented for $a = -1.0, 0.0$ and 1.0 . It is shown that the anisotropy factor a has not an appreciable effect on the temperature distribution in the medium.



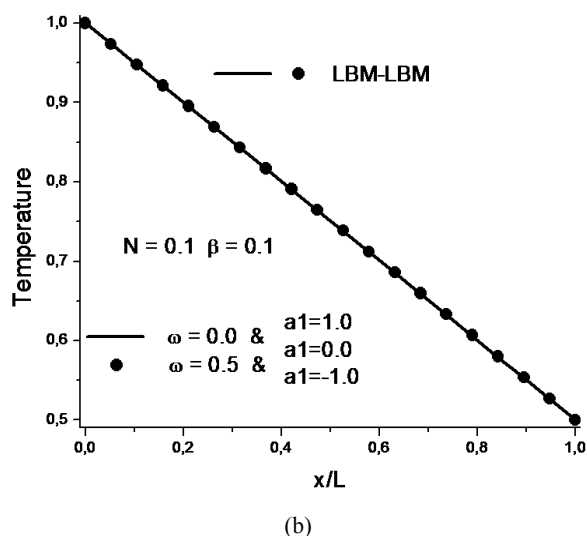


Fig. 7 Effect of the anisotropy factor a on non dimensional temperature T/T_w for (a) $\beta = 1.0$ (b) $\beta = 0.1$

IV. CONCLUSION

Combined conduction–radiation problem in one-dimensional gray planar absorbing, emitting and anisotropically scattering medium has been investigated by the LBM. In order to examine the accuracy and the computational efficiency of the proposed method, the non-dimensional temperature (T/T_w) is compared with the published results for various values of the extinction coefficient, conduction–radiation parameter, boundary emissivity, scattering albedo, anisotropy factor and east boundary temperature. For all cases studied, a good agreement is obtained.

REFERENCES

- [1] W. Yuen, E. Takara. "Analysis of combined conductive-radiative heat transfer in a two dimensional rectangular enclosure with a grey medium". *Trans ASME J Heat Transfer*, vol.110, pp. 468–474, 1988.
- [2] TY. Kim, SW. Baek. "Analysis of combined conductive and radiative heat transfer in a two-dimensional rectangular enclosure using the discrete ordinates method". *Int J Heat Mass Transfer*, vol.34, pp. 2265–2273, 1991.
- [3] KH. Lee, R. Viskanta. "Two-dimensional combined conduction and radiation heat transfer: comparison of the discrete ordinates method and the diffusion approximation methods". *Numer Heat Transfer A*, vol.39, pp. 205–225, 2001
- [4] SC. Mishra, RR. Vernekar. "Analysis of transport of collimated radiation in a participating media using the lattice Boltzmann method", *J Quant Spectrsc RadiatTransfer*, vol.113, pp. 2088–2099, 2012.
- [5] RR. Nourgaliev, TN. Dinh, TG. Theofanous, D. Joseph "The Lattice Boltzmann Equation Method: Theoretical Interpretation Numerics and Implications", *Int. J. Multipase Flow*, vol.29, pp. 117–169, 2003.
- [6] S. Chen, GD. Doolen. "Lattice Boltzmann Method for Fluid Flows", *Annu. Rev. Fluid Mech*, vol. 30, pp. 329–364, 1998.
- [7] X. He, S. Chen, GD. Doolen. "A Novel Thermal Model for the Lattice Boltzmann Method in Incompressible Limit", *J. Comput. Phys*, vol. 146, pp. 282–300, 1998
- [8] DA. Wolf-Gladrow. "Lattice-Gas Cellular Automata and Lattice Boltzmann Models: An Introduction", Springer-Verlag, Berlin-Heidelberg, 2000.
- [9] S. Succi "The Lattice Boltzmann Equation for Fluid Dynamics and Beyond", Oxford University Press, New York, 2001.
- [10] R. Ho, CP. Kuo, WS. Jiaung, CJ. Twu. "Lattice Boltzmann Scheme for Hyperbolic Heat Conduction Equation, Numer". *Heat Transfer B*, vol. 41, pp. 591–607, 2002.

- [11] JR. Ho, CP. Kuo, WS. Jiaung. "Study of Heat Transfer in Multilayered Structure within the Framework of Dual-Phase-Lag Heat Conduction Model Using Lattice Boltzmann Method", *Int. J. Heat Mass Transfer*, vol.46, pp. 55–69, 2003.
- [12] WS. Jiaung, JR. Ho, CP. Kuo. "Lattice Boltzmann Method for Heat Conduction Problem with Phase Change", *Numer. Heat Transfer B*, vol.39, pp. 167–87, 2001.
- [13] S. Srinivasan, RS. Miller, E. Marotta "Parallel Computation of the Boltzmann Transport Equation for Microscale Heat Transfer in Multilayered Thin Films", *Numer. Heat Transfer B*, vol.46, pp. 31–58, 2004.
- [14] Z. Guo, TS. Zhao. "Lattice Boltzmann Simulation of Natural Convection with Temperature Dependent Viscosity in a Porous Cavity", *Prog. Comput. Fluid Dynam*, vol. 5, pp.110–117, 2005.
- [15] M. Jamia, A. Mezhaba, M. Bouzidib, P. Lallemand, "Lattice-Boltzmann Computation of Natural Convection in a Partitioned Enclosure with Inclined Partitions Attached to Its Hot Wall", *Physica A* vol.368, pp.481–494, 2006.
- [16] D. Chatterjee, Chakraborty .S. "An Enthalpy-Based Lattice Boltzmann Model for Diffusion Dominated Solid-Liquid Phase Transformation", *Phys. Lett. A*, vol. 341, pp. 320–330, 2005.
- [17] R. Raj, A. Prasad, PR. Parida, SC. Mishra, "Analysis of solidification of a semitransparent planar layer using the lattice Boltzmann method and the discrete transfer method", *Numer. Heat Transfer Part A*, vol 49, pp. 279–299, 2006.
- [18] SC. Mishra, HK. Roy, "Solving transient conduction–radiation problems using the lattice Boltzmann method and the finite volume method", *J. Comput. Phys*, vol.223, pp.89–107, 2007.
- [19] B. Mondal, SC. Mishra, "Application of the lattice boltzmann method and the discrete ordinates method for solving transient conduction and radiation heat transfer problems", *Numerical Heat Transfer, Part A*, vol.52, pp. 757–775, 2007
- [20] R. Chaabane, F. Askri, SB. Nasrallah. "Analysis of two-dimensional transient conduction–radiation problems in an anisotropically scattering participating enclosure using the lattice Boltzmann method and the control volume finite element method". *Comput Phys Commun*, vol. 182, 1402–1413, 2011.
- [21] P. Talukdar, SC. Mishra "Analysis of conduction–radiation problem in absorbing, emitting and anisotropically scattering media using the collapsed dimension method". *Int J of Heat and Mass Transfer*, vol.45, pp. 2159–2168, 2002
- [22] SC. Mishra, P. Talukdar, D. Trimis, F. Durst. "Computational efficiency improvements of the radiative transfer problems with or without conduction-a comparison of the collapsed dimension method and the discrete transfer method", *Int J of Heat and Mass Transfer*, vol.46, pp. 3083–3095, 2003.
- [23] WH. Sutton, "A Short Time Solution for Coupled Conduction and Radiation in a Participating Slab Geometry", *J. Heat Transfer*, vol.108, pp.465–466, 1986.
- [24] JH. Tsai, JD. Lin. "Transient Combined Conduction and Radiation with Anisotropic Scattering", *J. Thermo phys. Heat Transfer*, vol. 4, pp.92–97, 1990.