

An optimal control problem for rigid body motions on Lie group $SO(2, 1)$

Nemat Abazari, Ilgin Sager

Abstract—In this paper smooth trajectories are computed in the Lie group $SO(2, 1)$ as a motion planning problem by assigning a Frenet frame to the rigid body system to optimize the cost function of the elastic energy which is spent to track a timelike curve in Minkowski space. A method is proposed to solve a motion planning problem that minimize the integral of the square norm of Darboux vector of a timelike curve. This method uses the coordinate free Maximum Principle of Optimal control and results in the theory of integrable Hamiltonian systems. The presence of several conserved quantities inherent in these Hamiltonian systems aids in the explicit computation of the rigid body motions.

Keywords—Optimal control, Hamiltonian vector field, Darboux vector, Maximum Principle, Lie group, Rigid body motion, Lorentz metric

I. INTRODUCTION

AN optimal control problem is used for rigid body motions and formulation on Lie group $SO(2, 1)$ where the cost function to be minimized is equal to the integral of the norm of Darboux vector of a timelike curve. This problem is analogous to the elastic problem in [1], [4]. The coordinate free maximum principle [2], [3] is applied to solve this problem. In [4] the author applied an integrable case where the necessary conditions for optimality can be expressed analitically and the corresponding optimal motions are expressed in a coordinate free manner. These optimal motions are showed to trace helical paths. In this study, the optimal control problem formulation is considered as the general theory of optimal control for the motion planning application, framed curves and left-invariant Hamiltonian systems are applied to this particular setting. Frenet frame of curve is applied to the Lorentz-Minkowski space to solve the problem and a particular set of curves is analyzed that satisfy these necessary conditions and provide analytic solutions for the corresponding optimal motions. An application of the Maximum Principle to this problem results in a system of first order differential equations that yield coordinate free necessary conditions for optimality. This system minimizes the cost function of elastic energy which is spend to track a timelike curve in Minkowski space.

II. FRENET FRAME

The Lorentz-Minkowski space is the metric space $E^3 = (R^3, \langle, \rangle)$ where the metric is given by

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$$\langle x, y \rangle = +x_1y_1 + x_2y_2 - x_3y_3 \quad (1)$$

The exterior product is defined as $x \times y = (-y_2x_3 - x_2y_3)\vec{e}_1 + (y_3x_1 - x_3y_1)\vec{e}_2 + (y_2x_1 - x_2y_1)\vec{e}_3$ where $\vec{e}_1, \vec{e}_2, \vec{e}_3$ is the standard orthonormal frame in R^3 .

The metric \langle, \rangle is called as Lorentzian metric.

Let H^2 denote the hyperboloid $x_1^2 + x_2^2 - x_3^2 = 1, x_1 > 0$

The isometry group for a hyperbolic plane H^2 is denoted by $SO(2, 1)$. Recall that $SO(2, 1)$ is the group that leaves the bilinear form \langle, \rangle in E^3 invariant.

$$\langle Ax, y \rangle + \langle x, Ay \rangle = 0 \quad (2)$$

is satisfied for any 3×3 matrice A on the Lie algebra L of $SO(2, 1)$.

It is verified that L is equal to the space of matrices

$$A = \begin{bmatrix} 0 & -a_1 & a_2 \\ a_1 & 0 & a_3 \\ a_2 & a_3 & 0 \end{bmatrix} \quad (3)$$

Definition A vector $v \in E^3$ is called

$$1. \text{Spacelike if } \langle v, v \rangle > 0 \text{ or } v = 0 \quad (4)$$

$$2. \text{Timelike if } \langle v, v \rangle < 0$$

$$3. \text{Lightlike if } \langle v, v \rangle = 0 \text{ and } v \neq 0$$

Definition For a curve α in E^3 , α is spacelike (resp. timelike, lightlike) at t if $\alpha'(t)$ is a spacelike (resp. timelike, lightlike) vector. If it is for any $t \in I$, the curve α is called spacelike (resp. timelike, lightlike).

In this paper we suppose that α is a spacelike curve, we call $T(s) = \alpha'(s)$ as the tangent vector at s and we supposed $T(s) \neq 0$ is the spacelike vector independent with $T(s)$.

The curvature of α at s is defined as $k(s) = |T'(s)|$. The normal vector $N(s)$ is defined by

$$N(s) = \frac{T'(s)}{k(s)} = \frac{\alpha''(s)}{\alpha'(s)} \quad (5)$$

Moreover $k(s) = \langle T'(s), N(s) \rangle$ is the curvature of the curve α . The binormal vector $B(s)$ is defined by

$$B(s) = T(s) \times N(s) \quad (6)$$

$\tau(s) = -\langle N'(s), B(s) \rangle$ is the torsion of the curve α . For each s , $\{T, N, B\}$ is an orthonormal base of E^3 which is called the Frenet trihedron of α .

By differentiation each one of the vector functions of the frenet trihedron frame $R = (T | N | B) \in L$ about the curve $\alpha : I \rightarrow E^3$ described by the following differential equations:

$$\begin{aligned} \alpha'(t) &= T \\ T' &= kN \\ N' &= -kT + \tau B \\ B' &= \tau N \end{aligned} \quad (7) \quad A_1 = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}, A_2 = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} \quad (14)$$

where k curvature, τ torsion of the curve α [6]

$$\begin{bmatrix} T' \\ N' \\ B' \end{bmatrix} = \begin{bmatrix} 0 & k & 0 \\ -k & 0 & \tau \\ 0 & \tau & 0 \end{bmatrix} \begin{bmatrix} T \\ N \\ B \end{bmatrix} \quad (8) \quad A_3 = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 \end{bmatrix}, B_1 = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix} \quad (16)$$

These equations form a rotation motion with Darboux vector $w = \tau T - kB$ [5]. Also momentum rotation vector is expressed as follows:

$$\begin{aligned} T' &= w \times T \\ N' &= w \times N \\ B' &= w \times B \end{aligned} \quad (9)$$

where $|w|^2 = -\langle w, w \rangle = -(k^2 - \tau^2) = \tau^2 - k^2$.

In this study, this Frenet frame is used to plan rigid body motions by applying the Maximum Principle to optimal control systems defined on a Lie group [2]. An element $g(t) \in M$ is defined as:

$$g(t) = \begin{pmatrix} 1 & 0 \\ \alpha(t) & R(t) \end{pmatrix} \quad (10)$$

where $R(t) \in L$. There is also associated with (7) via the relations

$$\begin{aligned} [1 \ \alpha(t)]^T &= g(t) \vec{e}_1 \\ [0 \ T]^T &= g(t) \vec{e}_2 \\ [0 \ N]^T &= g(t) \vec{e}_3 \\ [0 \ B]^T &= g(t) \vec{e}_4 \end{aligned} \quad (11)$$

where $\vec{e}_1, \vec{e}_2, \vec{e}_3, \vec{e}_4$ is the standard orthonormal frame in E^4 .

Proposition 1 The left-invariant differential equation:

$$\frac{dg(t)}{dt} = g(t) \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & -k & 0 \\ 1 & k & 0 & \tau \\ 0 & 0 & \tau & 0 \end{pmatrix} \quad (12)$$

where $g(t) \in M$ is equivalent to the Frenet frame (7).

Proof: It follows from differentiating (11) w.r.t to t that

$$\begin{aligned} [1 \ \alpha(t)]^T &= \frac{dg(t)}{dt} \vec{e}_1 = g(t) \vec{e}_2 = [0 \ T]^T \\ [0 \ T]^T &= \frac{dg(t)}{dt} \vec{e}_2 = g(t) (k \vec{e}_3) = k [0 \ N]^T \\ [0 \ N]^T &= \frac{dg(t)}{dt} \vec{e}_3 = g(t) (-k \vec{e}_2 + \tau \vec{e}_4) \\ &= -k [0 \ T]^T + \tau [0 \ B]^T \\ [0 \ B]^T &= \frac{dg(t)}{dt} \vec{e}_4 = g(t) (\tau \vec{e}_3) = \tau [0 \ N]^T \end{aligned} \quad (13)$$

then equating the L.H.S to the R.H.S yields (7).

The system (12) can be expressed conveniently in coordinate form by defining the following basis for the Lie algebra of M denoted by m

$$B_2 = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}, B_3 = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad (18)$$

Using these notations, it follows that (12) can be expressed as:

$$\frac{dg(t)}{dt} = g(t)(B_2 - kA_1 + \tau A_3) \quad (19)$$

To minimize the elastic energy of the curve, this is equivalent minimizing the function:

$$J = \frac{1}{2} \int |w|^2 dt = \frac{1}{2} \int -\langle w, w \rangle dt = \frac{1}{2} \int (-k^2 + \tau^2) dt \quad (20)$$

where the w defined as the Darboux vector with the equation $w = \tau T - kB$.

The motion $g(t) \in M$ of the left-invariant differential system (15) which minimizes the expression (16) is computed on a given interval $[0, T]$ subject to the given boundary conditions $g(0) = g_0, g(T) = g_T$ on the next section.

III. HAMILTONIAN LIFT ON M

Due to the similarity in between optimal control problem and elastic problem, this optimal control problem is considered as elastic problem and the applicability of Maximum Principle is obvious. The Maximum Principle states that the optimal paths are the projections of the extremal curves onto the base manifold, where the extremal curves are solutions of certain Hamiltonian systems on the cotangent bundle. For the problem, the manifold is M and the cotangent bundle is T^*M . The appropriate pseudo-Hamiltonian on T^*M is defined as:

$$\begin{aligned} H(p, u, g) &= p(g(t) B_2) - kp(g(t) A_1) + \tau p(g(t) A_3) \\ &\quad - p_0 \frac{1}{2} (\tau^2 - k^2) \end{aligned} \quad (21)$$

where $p(\cdot) : TM \rightarrow \mathbb{R}$. In this study, the regular extremals where $p_0 = 1$ (ignoring abnormal extremals where $p_0 = 0$) is carried.

The cotangent bundle T^*M can be written as the direct product $M \times m^*$ where m^* is the dual of the Lie algebra m of M .

The original Hamiltonian defined on T^*M can be expressed as a reduced Hamiltonian on the dual of the Lie algebra m^* . The linear functions $M_i = \hat{p}(A_i), p_i = \hat{p}(B_i)$ for $i = 1, 2, 3$ where $\hat{p} : m \rightarrow \mathbb{R}$ are the Hamiltonian lifts of left-invariant vector fields on M , because $p(g(t) A_i) = \hat{p}(A_i)$ for any

$P = (g(t), \hat{p})$ and any $A_i \in m$. If M_i, p_i is a collection of linear functions generated by the basis A_i, B_i in m then the vector $(M_1, M_2, M_3, p_1, p_2, p_3)$ is the coordinate vector of \hat{p} relative to the dual basis A_i^*, B_i^* . The Hamiltonian (17) becomes

$$H = p_2 - kM_1 + \tau M_3 - \frac{1}{2}(\tau^2 - k^2) \quad (22)$$

It follows from [12] that calculating $\frac{\partial H}{\partial k} = \frac{\partial H}{\partial \tau} = 0$ yields the optimal controls:

$$k = M_1, \tau = M_3 \quad (23)$$

substituting (19) into (18) gives the optimal Hamiltonian:

$$H = p_2 + \frac{1}{2}(M_3^2 - M_1^2) \quad (24)$$

In addition substituting the expressions (19) into (12) the optimal motions are the solutions $g(t) \in M$ of the differential equation:

$$\frac{dg(t)}{dt} = g(t) \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & -M_1 & 0 \\ 1 & M_1 & 0 & M_3 \\ 0 & 0 & M_3 & 0 \end{pmatrix} \quad (25)$$

To solve the equation (21) for $g(t) \in M$, it is necessary to solve the ekstremal curves M_1, M_2, M_3 for a special case.

IV. SOLVING THE EXTREMAL CURVES

To compute the corresponding Hamiltonian vector fields from the left-invariant Hamiltonian (20) the Lie bracket table (a) obtained for the basis (14):

[,]	A_1	A_2	A_3	B_1	B_2	B_3
A_1	0	$-A_3$	A_2	0	B_3	B_2
A_2	A_3	0	A_1	B_3	0	B_1
A_3	$-A_2$	$-A_1$	0	B_2	B_1	0
B_1	0	$-B_3$	$-B_2$	0	0	0
B_2	$-B_3$	0	$-B_1$	0	0	0
B_3	$-B_2$	$-B_1$	0	0	0	0

table (a)

where the Lie Bracket is defined as $[X, Y] = XY - YX$.

The time derivatives of M_i, p_i along the Hamiltonian flow are described by the Poisson bracket given by the equation:

$$\left\{ \hat{p}(\cdot), \hat{p}(\cdot) \right\} = -\hat{p}([\cdot, \cdot]) \quad (26)$$

$$\begin{aligned} M_1' &= \{M_1, H\} = \left\{ M_1, p_2 + \frac{1}{2}(M_3^2 - M_1^2) \right\} \\ &= \{M_1, p_2\} + M_3 \{M_1, M_3\} - M_1 \{M_1, M_1\} \\ &= -p_3 - M_3 M_2 \end{aligned}$$

$$\begin{aligned} M_2' &= \{M_2, H\} = \left\{ M_2, p_2 + \frac{1}{2}(M_3^2 - M_1^2) \right\} \\ &= \{M_2, p_2\} + M_3 \{M_2, M_3\} - M_1 \{M_2, M_1\} \\ &= 0 \end{aligned}$$

$$\begin{aligned} M_3' &= \{M_3, H\} = \left\{ M_3, p_2 + \frac{1}{2}(M_3^2 - M_1^2) \right\} \\ &= \{M_3, p_2\} + M_3 \{M_3, M_3\} - M_1 \{M_3, M_1\} \\ &= -p_1 - M_1 M_2 \end{aligned}$$

$$\begin{aligned} p_1' &= \{p_1, H\} = \left\{ p_1, p_2 + \frac{1}{2}(M_1^2 - M_3^2) \right\} \\ &= \{p_1, p_2\} + M_1 \{p_1, M_1\} - M_3 \{p_1, M_3\} \\ &= -p_2 M_3 \end{aligned}$$

$$\begin{aligned} p_2' &= \{p_2, H\} = \left\{ p_2, p_2 + \frac{1}{2}(M_1^2 - M_3^2) \right\} \\ &= \{p_2, p_2\} + M_1 \{p_2, M_1\} - M_3 \{p_2, M_3\} \\ &= p_1 M_3 + p_3 M_1 \end{aligned}$$

$$\begin{aligned} p_3' &= \{p_3, H\} = \left\{ p_3, p_2 + \frac{1}{2}(M_1^2 - M_3^2) \right\} \\ &= \{p_3, p_2\} + M_1 \{p_3, M_1\} - M_3 \{p_3, M_3\} \\ &= p_2 M_1 + p_1 M_2 \end{aligned}$$

The Hamiltonian vector fields are

$$M_1' = -p_3 - M_3 M_2$$

$$M_2' = 0$$

$$M_3' = -p_1 - M_1 M_2$$

$$p_1' = -p_2 M_3$$

$$p_2' = p_1 M_3 + p_3 M_1$$

$$p_3' = p_2 M_1$$

A trivial example of an integrable case of vector fields (24) occurs when $p_1 = p_2 = p_3 = M_1 = M_2 = M_3 = 0$. Moreover, for these values $p_1 = p_2 = p_3 = M_1 = M_2 = M_3$ are constant $\forall t$ and therefore the system is integrable. Substituting these values into (15)

$$\frac{dg(t)}{dt} = g(t) B_2 \quad (27)$$

this is easily integrated to yield $\alpha(t) = [t, 0, 0]^T$ with R equal to a 3×3 matrix with zero entries. Therefore, a straight line motion with zero rotation about this line is an optimal rigid body motion. In addition there exists a nontrivial integrable case of the Hamiltonian vector fields (24). This case is considered nontrivial as it gives rise to time-dependent extremal curves. It is observed that $p_1 = p_2 = p_3 = 0$ is

an invariant surface for the Hamiltonian vector fields (24). Explicitly, for $p_1 = p_2 = p_3 = 0$ the equations (24) degenerate to:

$$\begin{aligned} M_1' &= -M_3 M_2 \\ M_2' &= 0 \\ M_3' &= -M_1 M_2 \end{aligned}$$

$$\begin{aligned} p_1' &= 0 \\ p_2' &= 0 \\ p_3' &= 0 \end{aligned}$$

this implies that M_2 is constant that will be denoted by c . In addition $p_1 = p_2 = p_3 = 0 \forall t$. It follows that the Hamiltonian vector fields (26) are completely integrable. For these particular curves the Hamiltonian (20) reduces to

$$H = M_3^2 - M_1^2 \quad (28)$$

It follows that the differential equations (26) are satisfied that the extremal curves are:

$$\begin{aligned} M_2 &= c \\ M_1 &= r \cosh ct \\ M_3 &= -r \sinh ct \end{aligned} \quad (29)$$

To compute the optimal motions corresponding to the extremal curves (28) is not trivial as the elements of the Lie algebra are time-dependent.

V. OPTIMAL MOTIONS FOR THE RIGID BODY

The geodesic frame (21) is split into its translational and rotational part:

$$\frac{d\alpha(t)}{dt} = R\vec{e}_1 \quad (30)$$

and

$$\frac{dR}{dt} = R \begin{bmatrix} 0 & -M_1 & 0 \\ M_1 & 0 & M_3 \\ 0 & M_3 & 0 \end{bmatrix} \quad (31)$$

where $R^{-1} = R^T$. A basis is described for the Lie algebra m as:

$$\begin{aligned} E_1 &= \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}, E_2 = \begin{bmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{bmatrix}, \\ E_3 &= \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & 1 & 0 \end{bmatrix} \end{aligned} \quad (32)$$

The quantities

$$RPR^{-1} = \text{constant} \quad (33)$$

and

$$RMR^{-1} + [X, RPR^{-1}] = \text{constant} \quad (34)$$

are conserved for all left-invariant Hamiltonian systems on M where

$$\begin{aligned} M &= M_1 E_1 + M_2 E_2 + M_3 E_3 \\ P &= p_1 E_1 + p_2 E_2 + p_3 E_3 \\ X &= x_1 E_1 + x_2 E_2 + x_3 E_3 \end{aligned} \quad (35)$$

where x_1, x_2, x_3 are the position coordinates of the vector $\alpha(t) = [x_1, x_2, x_3]^T$.

Using these constants of motion (30) is integrated which is stated in the following theorem:

Theorem 3: $R = (T | N | B) \in L$ is the optimal rotation matrix corresponding to the extremals (28) which relates the Frenet frame to a fixed inertial frame where:

$$\begin{aligned} T &= \begin{bmatrix} \cosh Kt \cosh ct - \frac{c}{K} \sinh Kt \sinh ct \\ \frac{r}{K} \sinh ct \\ \sinh Kt \cosh ct + \frac{c}{K} \cosh Kt \sinh ct \end{bmatrix} \\ N &= \begin{bmatrix} -\frac{r}{K} \sinh Kt \\ \frac{c}{K} \\ -\frac{r}{K} \cosh Kt \end{bmatrix} \\ B &= \begin{bmatrix} -\cosh Kt \sinh ct + \frac{c}{K} \sinh Kt \cosh ct \\ -\frac{r}{K} \cosh ct \\ -\sinh Kt \sinh ct + \frac{c}{K} \cosh Kt \cosh ct \end{bmatrix} \end{aligned}$$

where $K^2 = c^2 - r^2$ and r, c are the constant parameters of the curvatures (28).

Proof For these particular curves $p_1 = p_2 = p_3 = 0$ the conservation laws (32) and (33) reduce to:

$$RMR^{-1} = \text{constant} \quad (36)$$

this constant matrix RMR^{-1} is then conjugated for a particular solution R such that:

$$RMR^{-1} = \sqrt{M_1^2 + M_2^2 - M_3^2} E_2 \quad (37)$$

substituting (24) into (37) gives

$$RMR^{-1} = \sqrt{c^2 - r^2} E_2 \quad (38)$$

The constant K is defined with the equation: $K^2 = c^2 - r^2$. Therefore

$$M = KR^{-1} E_2 R \quad (39)$$

is verified. Expressing R in a convenient coordinate from [12]:

$$R = \exp(\varphi_1 E_2) \exp(\varphi_2 E_3) \exp(\varphi_3 E_2) \quad (40)$$

and substituting (40) into (39) yields:

$$M = K \exp(-\varphi_3 E_2) \exp(-\varphi_2 E_3) E_2 \exp(\varphi_2 E_3) \exp(\varphi_3 E_2) \quad (41)$$

It is shown that:

$$M = K \begin{bmatrix} 0 & \sinh \varphi_2 \cosh \varphi_3 & \cosh \varphi_2 \\ -\sinh \varphi_2 \cosh \varphi_3 & 0 & -\sinh \varphi_2 \sinh \varphi_3 \\ \cosh \varphi_2 & -\sinh \varphi_2 \sinh \varphi_3 & 0 \end{bmatrix} \quad (42)$$

equating M in (34) to (42) gives:

$$M_1 = -K \sinh \varphi_2 \cosh \varphi_3 \quad (43)$$

$$M_2 = K \cosh \varphi_2$$

$$M_3 = -K \sinh \varphi_2 \sinh \varphi_3$$

So it is easily shown that:

$$\cosh \varphi_2 = \frac{M_2}{K} = \frac{c}{K} \quad (44)$$

$$\sinh \varphi_2 = \mp \sqrt{\frac{c^2}{K^2} - 1} = \mp \frac{r}{K}$$

in addition form (43) we have:

$$\tanh \varphi_3 = \frac{M_3}{M_1} \quad (45)$$

therefore

$$\sinh \varphi_3 = \mp \frac{M_3}{\sqrt{M_1^2 - M_3^2}} = \mp \sinh ct \quad (46)$$

$$\cosh \varphi_3 = \pm \frac{M_1}{\sqrt{M_1^2 - M_3^2}} = \cosh ct$$

in order to obtain an expression for φ_1 , we substitute (40) into (30) yields:

$$\frac{dR}{dt} = \varphi_1' E_2 \exp(\varphi_1 E_2) \exp(\varphi_2 E_3) \exp(\varphi_3 E_2) \quad (47)$$

$$+ \varphi_2' \exp(\varphi_1 E_2) E_3 \exp(\varphi_2 E_3) \exp(\varphi_3 E_2)$$

$$+ \varphi_3' \exp(\varphi_1 E_2) \exp(\varphi_2 E_3) E_2 \exp(\varphi_3 E_2)$$

therefore

$$R^{-1} \frac{dR}{dt} = \varphi_1' \exp(-\varphi_3 E_2) \exp(-\varphi_2 E_3) E_2 \exp(\varphi_2 E_3) \exp(\varphi_3 E_2) \quad (48)$$

$$+ \varphi_2' \exp(-\varphi_3 E_2) E_3 \exp(\varphi_3 E_2)$$

$$+ \varphi_3' E_2$$

$$= \varphi_1' \begin{bmatrix} 0 & \sinh \varphi_2 \cosh \varphi_3 & \cosh \varphi_2 \\ -\sinh \varphi_2 \cosh \varphi_3 & 0 & -\sinh \varphi_2 \sinh \varphi_3 \\ \cosh \varphi_2 & -\sinh \varphi_2 \sinh \varphi_3 & 0 \end{bmatrix} \frac{1}{k^2} [-r \cosh kt, ct, -r \sinh kt]^T$$

$$+ \varphi_2' \begin{bmatrix} 0 & -\sinh \varphi_3 & 0 \\ \sinh \varphi_3 & 0 & \cosh \varphi_3 \\ 0 & \cosh \varphi_3 & 0 \end{bmatrix}$$

$$+ \varphi_3' \begin{bmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{bmatrix}$$

$$= \begin{bmatrix} 0 & -M_1 & 0 \\ M_1 & 0 & M_2 \\ 0 & M_2 & 0 \end{bmatrix}$$

which leads to

$$-M_1 = \varphi_1' \sinh \varphi_2 \cosh \varphi_3 - \varphi_2' \sinh \varphi_3 \quad (49)$$

$$M_3 = -\varphi_1' \sinh \varphi_2 \sinh \varphi_3 + \varphi_2' \cosh \varphi_3$$

therefore

$$\varphi_1' = \frac{M_3 \sinh \varphi_3 - M_1 \cosh \varphi_3}{\sinh \varphi_2} \quad (50)$$

substituting (28), (44) and (46) into (50) yields:

$$\varphi_1' = K \quad (51)$$

and integrating with respect to t yields:

$$\varphi_1 = Kt + \beta \quad (52)$$

where β is a constant of integration and for $\beta = 0$ yields:

$$\varphi_1 = Kt \quad (53)$$

An other hand from (40) yields :

$$T = \begin{bmatrix} \cosh \varphi_1 \cosh \varphi_3 + \sinh \varphi_1 \cosh \varphi_2 \sinh \varphi_3 \\ \sinh \varphi_2 \sinh \varphi_3 \\ \sinh \varphi_1 \cosh \varphi_3 + \cosh \varphi_1 \cosh \varphi_2 \sinh \varphi_3 \end{bmatrix} \quad (54)$$

$$N = \begin{bmatrix} \sinh \varphi_1 \sinh \varphi_2 \\ \cosh \varphi_2 \\ \cosh \varphi_1 \sinh \varphi_2 \end{bmatrix}$$

$$B = \begin{bmatrix} \cosh \varphi_1 \sinh \varphi_3 + \sinh \varphi_1 \cosh \varphi_2 \cosh \varphi_3 \\ \sinh \varphi_2 \cosh \varphi_3 \\ \sinh \varphi_1 \sinh \varphi_3 + \cosh \varphi_1 \cosh \varphi_3 \cosh \varphi_2 \end{bmatrix}$$

substituting (44) , (46) and (52) into (55) yields $R = (T | N | B)$.

Lemma: The optimal path $\alpha(t) \in E^3$ defined by the differential equation (29), with $M_1 = r \cosh ct$, $M_2 = c$ and $M_3 = -r \sinh ct$ described by:

$$\frac{d\alpha(t)}{dt} = \frac{1}{k} \begin{bmatrix} -r \sinh kt \\ c \\ -r \cosh kt \end{bmatrix}$$

$$\alpha(t) = \frac{1}{k} \int \begin{bmatrix} -r \sinh kt \\ c \\ -r \cosh kt \end{bmatrix} dt = \frac{1}{k^2} [-r \cosh kt, ct, -r \sinh kt]^T$$

$$\frac{d\alpha(t)}{dt} = \frac{1}{k} \begin{bmatrix} -r \sinh kt \\ c \\ -r \cosh kt \end{bmatrix}$$

$$\alpha(t) = \frac{1}{k} \int \begin{bmatrix} -r \sinh kt \\ c \\ -r \cosh kt \end{bmatrix} dt =$$

VI. ACKNOWLEDGMENT

The authors wish to express his/her gratitude to an anonymous referees whose comments and suggestions proved most constructive, informative and useful during the revision of this manuscript.

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