Abstract—As the electrical power industry is restructured, the electrical power exchange is becoming extended. One of the key information used to determine how much power can be transferred through the network is known as available transfer capability (ATC). To calculate ATC, traditional deterministic approach is based on the severest case, but the approach has the complexity of procedure. Therefore, novel approach for ATC calculation is proposed using cost-optimization method in this paper, and is compared with well-being method and risk-benefit method. This paper proposes the optimal transfer capability of HVDC system between mainland and a separated island in Korea through these three methods. These methods will consider production cost, wheeling charge through HVDC system and outage cost with one depth (N-1 contingency).

Keywords—ATC, Power system interconnection, well-being method, cost-optimization method, risk-benefit analysis, outage cost

I. INTRODUCTION

In deregulated power market, system operators require efficient methods to calculate optimal transfer capability between two or more areas. Available transfer capability (ATC) of the transmission system is introduced by the United States Federal Energy Regulatory commission (FERC). The ATC is the reserved capability of transmission lines at a given time and varies from hour to hour based on the many factors. For example, the ATC is affected by generation dispatch, demand level, transfer capability between two areas, network topology and the limits on the transmission line. In the transmission system, optimal operation is dependent upon the ATC.

In Korea, mainland and a separated island are interconnected by HVDC. KEPCO (Korean Electric Power Corporation) has restructured the power industry and attempted to increase economic efficiency of the interconnection within reliability criteria. This paper proposes a cost-optimization method to obtain optimal ATC and the method is compared with well-being method and risk-benefit method. The well-being method is one of the reliability assessment techniques and the risk-benefit method is one of the economic assessment techniques to obtain optimal ATC. The three methods use Local Marginal Price (LMP) of transfer capability between interconnected systems, production cost in generators and outage cost considering N-1 contingency. Data used in case study is LMP, generation data and demand of separated island in June 2008.

II. ATC AND THREE METHODS

A. Determination of Available Transfer Capability

By the NERC definition [1], ATC is determined by several parameters, namely, Total Transfer Capability (TTC), Transmission Reliability Margin (TRM), Existing Transmission Commitment (ETC), and Capacity Benefit Margin (CBM).

\[
\text{TTC} = \text{Min}\left(\frac{\text{Thermal Limit}}{\text{Voltage Limit}} \times \text{Stability Limit} \times \text{Stability Limit} \times \text{Stability Limit} \times \text{Stability Limit} \right)
\]

\[
\text{ATC} = \text{TTC} - \text{TRM} - \text{ETC} - \text{CBM}
\]

B. Determination of cost-optimization method

Cost-optimization method is one of ATC calculation method, and is used to calculate optimal transfer capability in this paper. The computation of total cost through cost calculation can be expressed as Eq. (3). [2]
\[ \min [C] = C_G + C_W + C_O \]  

where, 
- C : Total cost\[\text{₩}\],  
- \(C_G\) : Production cost of generators \[\text{₩/MW}\]  
- \(C_W\) : Wheeling charge\[\text{₩/MW}\]  
- \(C_O\) : Outage cost\[\text{₩/MW}\]

### Calculation of production cost

Production cost consists of fixed and changeable costs. Usually, fixed cost is relatively less than changeable one. It is assumed fuel cost equals production cost, because the changeable fuel cost takes the most part of expense composition.

Eq. (7) means production cost.

\[ C_p(t) = \sum_{i=1}^{k(t)-1} \left( G_i \times g_i \right) + \left[ D(t) \left( T(t) + \sum_{i=1}^{k(t)-1} G_i \right) \right] \times g_k(t) \]  

where,  
- \(k(t)\) : number of generating generators at time \(t\)  
- \(G_i\) : maximum capability of \(i\)th generator [MW]  
- \(g_i\) : \(i\)th generator’s production cost per MW [\(\text{₩/MW}\)]  
- \(D(t)\) : demand level [MW]

### Calculation of outage cost

Outage cost can be obtained by two courses. Firstly, it is damage of customer who is not supplied electric power by contingency. Secondly, it is restoration expenditure and amount of reduction money due to contingency. [3]

In this paper, the interruption cost by economic activity is formulated as Eq. (4).

\[ C_e = \frac{\text{Value added by economic activity}}{\text{Power input by economic activity}} \]  

Calculation of outage cost can be represented as Eq. (5).

\[ C_o(t) = \text{ENS}(t) \times C_e \]  

where, \(\text{ENS}(t)\) : expected not supplied energy at time \(t\) [MWh]
- \(C_e\) : consumed electric energy by GNP [\(\text{₩/MWh}\)]

### Calculation of wheeling charge

Wheeling charge through interconnection line is decided by LMP and transfer capability.

\[ C_w(t) = \text{LMP}(t) \times T(t) \]  

where,  
- \(\text{LMP}(t)\) : local marginal price at time \(t\) [\(\text{₩/MW}\)]  
- \(T(t)\) : transfer capability in interconnection line [MW]

### Calculation of well-being method

Concepts of the basic probabilistic method designated as the EPRI method [4] are illustrated in detail in Reference 5. The main advantage of the well-being method is that it combines deterministic considerations and probabilistic indices of systems as well. [6]

### Approach well-being method

Process of reliability assessment in the well-being method is begun from the evaluation of ‘At risk’ state. When outage happens, system state is transferred to ‘Marginal’ state or ‘At risk’ state. The first step considers every outage and outage probability, and calculates ‘At risk’ probability. The second step calculates ‘Healthy’ probability in keeping their operating condition. Finally, ‘Marginal’ probability can be calculated, since the summation of every probability is 1.

\[ P_m = 1 - \left( P_h + P_r \right) \]  

where,  
- \(P_m\) : ‘Marginal’ state probability,  
- \(P_h\) : ‘Healthy’ state probability  
- \(P_r\) : ‘At risk’ state probability.

\[ P_r = 1 - \sum_{i=1}^{n} P_i \]  

\[ P_h = \sum_{i=1}^{n} P_i^2 \]
\[ P_m = \bigcup_{i=1}^{n} P_i - \bigcup_{i=1}^{n} P_i^2 \] (11)

where, \( n \) : number of components in system

**D. Determination of risk-benefit method**

- **Benefit function**

  Benefit function is the sum of four-kind functions. First, profit from transmission system may be exposed by transmission owner’s profits-increase. Second, transfer capability enlargement can delay a required transmission system expansion due to the increased load demand. Benefit function also includes those delayed expansions. Third benefit can be calculated by the profit of utilities. Forth, benefit function includes power loss due to transfer capability \([7]\).

Now, Benefit function is:

\[ B(T) = \alpha_w \cdot B_w(T) + \alpha_e \cdot B_e(T) + \alpha_u \cdot B_u(T) - \alpha_l \cdot C_l(T) \] (12)

\[ B_w(T) = \text{LMP}_{av} \times T \]

\[ B_e(T) = C_d \times e^{\frac{r_\text{av}}{T}} \]

\[ B_u(T) = C_s \times (D_{av} - T) \]

\[ C_l = K_i \cdot \beta_i \cdot T \] (13)

where, \( \alpha_w, \alpha_e, \alpha_u, \alpha_l \) : weighting factor

\( B_w \) : Benefits in power market

\( T \) : transfer capability [MW] : \( 0 \leq T \leq 300\text{[MW]} \)

\( \text{LMP}_{av} \) : Average LMP [\$/MWh]

\( B_e \) : Benefits of delayed a transmission expansion

\( C_d \) : Capital delayed a transmission system expansion

\( r_\text{av} \) : Annual rate of interest

\( Y_s \) : Year of delayed a transmission expansion

\( D_{av} \) : Rate of demand growth

\( B_u \) : Benefit of utility

\( C_s \) : Customer price [\$/MWh]

\( D_{av} \) : Average Demand [MW]

\( C_l \) : Power loss of transfer capability [MW]

\( K_i \) : cost value of power loss [\$/MWh]

\( C_l \) : Rate of power and power loss

- **Risk function**

  Due to the complicated power system, risk function is represented in probabilistic function form. Risk function includes outage cost, generating cost for outage capability and power loss cost.

Risk function is expressed as

\[ R(T) = O(T, T_p) \cdot \text{FOR}_{\text{interconnection}} \] (14)

\[ O(T, T_p) = \alpha_e \cdot C_e (T - T_p) + \alpha_s \cdot C_s (T - T_p) + \alpha_l \cdot C_l(T_p) \] (15)

where, \( \alpha_e, \alpha_s, \alpha_l \) : weighting factor

\( T_p \) : Transfer capability after outage

\( \text{FOR}_{\text{interconnection}} \) : Forced outage rate of interconnection lines

**III. CASE STUDY**

**A. Overview of Jeju in Korea**

Jeju is biggest island in Korea, and is supplied 40% of present demand from mainland. If production cost of generators is higher than market price in mainland, island should receive more power. On the contrary, if LMP is more expensive than production cost and island has enough generation capability, island can supply electric power to mainland.

In June 2008, demand increases about 10 [%] per year, and production cost is about 3-4 times of LMP. Demand was low in daybreak and peak load happened at 22 hours. Average demand was 295-410[MW].

There are 4 power plants and 9 generators in separated
island. Production cost and capability of all generators are shown in Fig 3.

![Generating Capability and Cost in generators](image)

Fig 3. Generating Capability and Cost in generators

**B. Determination of cost-optimization method**

Now, it is assumed that HVDC system is used by 0[%], 50[%] and 100[%] of maximum capability.

- **Case 1. 0[%] usage of HVDC system**
  Without transfer capability through HVDC system, 9 generators supply total demand of island. Jeju #2, #3, ST and Nam Jeju #3 always supply power. Nam Jeju #4 and Nam Jeju ST operate timely according to demand. Hanrim GT, CC and Jeju GT #3, however, are the reserve capability.
  Calculation of production cost considers generator operating hours, minimal generating capability, starting cost, starting time and production cost per MW.
  Outage cost supposes contingency of Nam Jeju #3 which has biggest generating capability, and considers starting time of other generator.

- **Case 2. 50[%] usage of HVDC system**
  Transfer capability through HVDC system is 150 [MW] that is 50% of maximum rating. Jeju #2, #3, ST and HVDC always supply power, and other generators are the reserve capability.
  Two events are assumed to measure outage cost.
  - **Event A**: Contingency occurs in one line of HVDC system,
  - **Event B**: Contingency occurs in Jeju #3 and Jeju ST.

- **Case 3. 100[%] usage of HVDC system**
  In this case, HVDC system is fully used as much as maximum rating. As demand exceeds 300 [MW] Jeju #2 and #3, which have the lowest production cost per MW, should supply power.
  Two events are assumed to measure outage cost.
  - **Event A** – Contingency occurs in one line of HVDC system,
  - **Event B** – Contingency occurs in both lines of HVDC system.

**Computation of optimal transfer capability**

![Computation of optimal capability using cost-optimization](image)

Fig 4. Computation of optimal capability using cost-optimization

**C. Determination of well-being method**

In well-being method, when demand is flat, sum of state probability is 1. According to the variation of system condition, well-being method can calculate each state probability.

**Table 2. Outage rate of island’s power supply**

<table>
<thead>
<tr>
<th>Supplier</th>
<th>Capacity</th>
<th>FOR</th>
</tr>
</thead>
<tbody>
<tr>
<td>HVDC system</td>
<td>300 MW</td>
<td>3.8 %</td>
</tr>
<tr>
<td>Hanrim C/C</td>
<td>105 MW</td>
<td>7 %</td>
</tr>
<tr>
<td>Jeju #2, #3</td>
<td>150 MW</td>
<td>5 %</td>
</tr>
<tr>
<td>Jeju GT #3</td>
<td>55 MW</td>
<td>6 %</td>
</tr>
<tr>
<td>Nam Jeju GT</td>
<td>200 MW</td>
<td>5 %</td>
</tr>
</tbody>
</table>

![Computation of optimal capability using well-being method](image)

Fig 5. Computation of optimal capability using well-being method

Optimal transfer capability of HVDC system is 155–215[MW] in the well-being method.

**D. Determination of Risk-Benefit method**

Benefit function is expressed as Eq. (18).
\[ B(T) = a_{1}B_{w}(T) + a_{2}B_{c}(T) + a_{3}B_{r}(T) \]
\[ = LMP \cdot T + C_{0} \left( \frac{T}{T_{0}} \right)^{1} + 1948T + 1680 \]  
(18)

Fig. 6 shows that transfer capability using risk-benefit method of HVDC system, and the optimal value is 180 [MW].

E. Comparison of three methods

Cost-optimization method is compared with well-being method and risk-benefit method which considers reliability and economic aspect, respectively.

<table>
<thead>
<tr>
<th>Method</th>
<th>Optimal transfer capability</th>
</tr>
</thead>
<tbody>
<tr>
<td>Cost-optimization</td>
<td>150 ~ 225 [MW]</td>
</tr>
<tr>
<td>Well-being method</td>
<td>155 ~ 215 [MW]</td>
</tr>
<tr>
<td>Risk-benefit method</td>
<td>180 [MW]</td>
</tr>
</tbody>
</table>

The cost-optimization method considers reliability and economic assessments, while the well-being method considers only reliability assessment. The result of proposed method exists within the result of the well-being method. Also, the cost-optimization method optimizes hourly transfer capability, while the risk-benefit method shows only one optimal value.

IV. Conclusion

In response to the conflicting interests of various market participants and the demand of power system operators for enhancement of power system operation, this paper proposed equations designed to apply cost-optimization method to calculation and evaluation of optimal transfer capability. The method uses LMP of transfer capability between interconnected systems, production cost in generators and outage cost considering N-1 contingency. In the case study, the method is compared with well-being method and risk-benefit method to show merits. The result of cost-optimization method exists within optimal transfer capability using reliability assessment, and shows hourly optimal transfer capability compared with optimal value of economic method.

REFERENCES