Power System Voltage Control using LP and Artificial Neural Network

A. Sina, A. Aeenmehr, H. Mohamadian

Abstract-Optimization and control of reactive power distribution in the power systems leads to the better operation of the reactive power resources. Reactive power control reduces considerably the power losses and effective loads and improves the power factor of the power systems. Another important reason of the reactive power control is improving the voltage profile of the power system. In this paper, voltage and reactive power control using Neural Network techniques have been applied to the 33 shines-Tehran Electric Company. In this suggested ANN, the voltages of PQ shines have been considered as the input of the ANN. Also, the generators voltages, tap transformers and shunt compensators have been considered as the output of ANN. Results of this techniques have been compared with the Linear Programming. Minimization of the transmission line power losses has been considered as the objective function of the linear programming technique. The comparison of the results of the ANN technique with the LP shows that the ANN technique improves the precision and reduces the computation time. ANN technique also has a simple structure and this causes to use the operator experience.

Keywords—voltage control, linear programming, artificial neural network, power systems

I. INTRODUCTION

In a stable power system, the total loads and the power losses should be equal with the generated power. The variation of the reactive power will change the bus voltages. Thus keeping the voltage at a constant value is an important factor for the stability of the power system [6]. It is important to notice that load type and its variations are more major factors in the voltage and reactive power control. Three major methods are used to control the voltage in the power system.

- 1- Changing the set point of generator exciters.
- 2- Changing the tap of the transformers
- 3- Using the shunt compensators

In the first method, thermal limits of the generator windings are considered as a constraint to limit the generated and consumed reactive power of the generators.

Thus in the recent years, a lot of studies have been taken out for the modern reactive power and voltage control as a term for the improvement of the reliability and the stability in the power systems [2][3][12]. These methods have been introduced for solution of the reactive power and voltage control optimisation problem. To solve this problem, the mathematical optimisation methods have been used. Methods for reactive power and voltage control could be categorised into two major categories: methods based on the algorithmic methods and the methods based on the artificial intelligence. In this paper, the Linear Programming technique is selected as algorithmic method, and Artificial Neural Network technique is selected as an artificial intelligence method [1][11][13]. The data of the 33-shines of the Tehran Electric company have been used for the solution of the problem of the reactive power and voltage control by these two method and they have been compared with each other.

II. LINEAR PROGRAMMING METHOD

Recently High speed, reliability and precision of the Linear Programming (LP), causes it to be used in the power system networks as a very effective and reliable method for the optimization problems. In this method, reactive power sources and transformer taps are as the control variables and bus voltages and the reactive power of the generators are as the related variables. Linear Programming problems are made using the sensitivity relations based on the Newton-Raphson power flows. The objective function is minimization of the power losses and improvement of the voltage profiles [9].

The relation between the control variables and the voltage buses are made using the load models and the transformer taps and Jacobean matrixes. This relation also define the relation between the variables and the reactive power connected to the busses

Minimize:
$$\Delta P_L = L^T \Delta V$$

Subject to: $\Delta Q_{\min} \leq A \Delta V \leq \Delta Q_{\max}$

 ΔP_L : Variations of Transmission losses L: Vector coefficients of objective function

 ΔV : Vector variations of Shines Voltage

 ΔQ : Vector variations of shines reactive power A: Conditional functions Coefficients matrix

This method results in reduction of calculation time and memory space. Artificial Neural Networks extensively have been considered in the optimization problems [4][7].

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David Rumelhart and James Mcland have revolutionized the ANN methods after the introduction of the Error Back Propagations based methods [7]. These methods are categorized as the dynamic methods processing on the experimental data, knowledge and the rules governing on their behavior, transform them to the network structure.

ANN with a parallel structure has a parallel and quick processing with the large data storage and non-linear mapping, as a great capability. After the network is trained by the initial cases, ANN could have a very good output for the practical inputs [7].

III. CASE STUDY

In this paper, the case study is the 33-buses Tehran power company network. This network has 71 transmission lines, 13 generators (one as the reference and others as the PV buses) and 20 PQ buses.

The control variables are

- a) bus voltages no. 1 to 13
- b) reactive power sources at buses 4, 15 and 28
- c) transformer taps of the lines 6-6, 7-9 and 4-8
- Controlled variables are as following below
 - a) Voltages of shines numbers 1 to13
 - b) Reactive source of shines numbers 4, 15, and 28
 - c) Tap transformers of lines numbers 6-6, 9-7, 4-8



Fig. 1 Tehran power company network

A. Linear Programming Implementation

Bus 1 has been selected as the reference bus and buses 2, 3... m have been selected as the PV buses and buses m+1 ...n have been selected as the PQ buses.

B. Equations and Constraints of Linear Programming Method

Equations and the constraints of the LP As it was mentioned in the section 2, system model and the objective function have been linearized using the elements of the Jacobean and the sensitivity Matrixes. The equations are as following:

$$\Delta P_{L} = \begin{bmatrix} \frac{\partial P_{L}}{\partial V_{1}} & \frac{\partial P_{L}}{\partial V_{2}} & \cdots & \frac{\partial P_{L}}{\partial V_{m}} & \frac{\partial P_{L}}{\partial Q_{m+x}} & \frac{\partial P_{L}}{\partial t_{ij}} \end{bmatrix} \begin{bmatrix} \Delta V_{1} \\ \Delta V_{2} \\ \vdots \\ \vdots \\ \Delta V_{m} \\ \Delta Q_{m+x} \\ \Delta t_{ij} \end{bmatrix} : m \qquad (1)$$

In a practical system, there are some constraints on the control variables and the related variables.

$$\Delta V_{i}^{\min} \langle \Delta V_{i} \langle \Delta V_{i}^{\max}, i = 1, 2, ..., m$$

$$\Delta t_{ij}^{\min} \langle \Delta t_{ij} \langle \Delta t_{ij}^{\max} \rangle$$

$$\Delta Q_{m+x}^{\min} \langle \Delta Q_{m+x} \langle \Delta Q_{m+x}^{\max} \rangle$$

$$\Delta V_{i}^{\max} = V_{i}^{\max} - V_{i}, \Delta V_{i}^{\min} = V_{i}^{\min} - V$$

$$\Delta t_{ij}^{\max} = t_{ij}^{\max} - t_{ij}, \Delta t_{ij}^{\min} = t_{ij}^{\min} - t_{ij}, \lambda t_{ij}^{\min} = t_{ij}^{\min} - t_{ij}, \lambda t_{ij}^{\min} = t_{ij}^{\min} - t_{ij}, \lambda t_{ij}^{\max} = t_{ij}^{\max} - t$$

$$\Delta Q_{m+x}^{\max} = Q_{m+x}^{\max} - Q_{m+x}, \Delta Q_{m+x}^{\min} = Q_{m+x}^{\min} - Q_{m+x}$$

$$\Delta Q_{Gi}^{\min} \langle \Delta Q_{Gi} \langle \Delta Q_{Gi}^{\max}, i = 1, 2, ..., m$$

$$\Delta V_{j}^{\min} \langle \Delta V_{j} \langle \Delta V_{j}^{\max}, j = m+1, ..., n$$

$$\Delta Q_{Gi}^{\max} = Q_{Gi}^{\max} - Q_{Gi}, \Delta Q_{Gi}^{\min} = Q_{Gi}^{\min} - Q_{Gi}$$

$$\Delta V_{Lj}^{\min} = V_{Lj}^{\max} - V_{Lj}, \Delta V_{Lj}^{\min} = V_{Lj}^{\min} - V_{Lj}$$
(3)

Finally the LP problem for the controlling of the reactive power and the voltage are as following.

C. Objective Function

The objective is to minimize the power losses by some control variables, tap transformers and the reactive power sources. Equations and the constraints have been discussed in the section 2 and 2.1.4.

Minimize:

$$\Delta P_{L} = \begin{bmatrix} \frac{\partial P_{L}}{\partial V_{1}} \dots \frac{\partial P_{L}}{\partial V_{m}} \frac{\partial P_{L}}{\partial Q_{m+x}} \frac{\partial P_{L}}{\partial t_{ij}} \end{bmatrix} \begin{pmatrix} \Delta V_{1} \\ \Delta V_{2} \\ \ddots \\ \ddots \\ \ddots \\ \Delta V_{m} \\ \Delta Q_{m+x} \\ \Delta t_{ij} \end{bmatrix}$$
(4)

Subject to:

D.Implementation of the ANN on Network

As it is seen in the Fig. 2, the ANN has three layers with 23 neurons in the input layer, 19 neurons in the output layer and 8 neurons in the middle layer.

Back Error Propagation methods have been used in the training technique. The output neurons are consisted of 13 neurons as the generators, 3 neurons for the transformers with a variable taps and 3 neurons as the reactive power sources. The number of input neurons are 23 as the same as the number of the PQ buses. The numbers of the middle neurons have been selected due to the different structures tested.



In a real power system the operational conditions are changed with the loads. Therefore, in the training of the designed ANN, the load has been varied gradually from 0% to 120% with the step of the 20%. Also the coherent variation of the loads on the buses has been applied to the loads from 75%

to 115% with the step of 10%. Then, the input and the outputs have been determined. Finally the best model has been selected for the ANN training.

Training inputs is normalized using the following relation [14]:

$$P_{n} = \frac{2(P - P_{\min})}{P_{\max} - P_{\min}} - 1$$
(5)

The outputs are also normalized using this relation [14]:

$$T_n = \frac{T}{T_{\text{max}}} \tag{6}$$

The results of LP and ANN methods are shown in the tables brought at last pages. Table 1 shows the results of the initial power flow.

IV. RESULTS

The results of LP and ANN methods are shown in the tables brought in the appendix. Table I shows the results of the initial power flow

Table II has initial information of proposed system and includes kindness of shines, load value and voltage of each shine. In tables III, IV and V the results from LP and ANN are compared when the load of all PQ shines were reduced to 75%. Also, the results from LP and ANN are compared at 115 load and shown in tables VI, VII and VIII. These tables include, the load value of shine in percent, initial voltage before and after optimization, final voltage after optimization with two proposed methods, tap transformers values between shines (4,8), (4,9), (6,5), reactive power source value in shines 4, 15, 28, system losses value, produced active power value of shine 1, produced reactive power value of shine 1 to 13 in three situations before optimization, after optimization by LP method and after implementation of ANN.

V.CONCLUSION

In grid with 33 shines, the reduction of loads to 75% results in increase of voltages of shines 7, 11, 12, 13 illegally. In all cases, LP method causes to return of voltages in allowable limit. So proposed method is applicable for shines where have faulty limits.

The ANN method is almost defected in shine 7 but grid response are satisfied the constraints well in other situations. For load of 115%, when the shines have not faulty limits the implementation of proposed optimization methods, result in reduction of losses and improvement of voltage profile so that the voltages of buses 4 and 6 are reduced.

Therefore, the proposed methods have good performance for profile improvement and loss reduction in non- faulty limits.

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			TABL	ΕI				21	Р	Q	75	1.0563	1.0653	1.0772
		INITIAL I	NFORMAT	ION OF	System			22	Р	Q	75	1.0627	1.0548	1.0394
Shine	Kindness	Produ	ction	Lo	bad	Voltage	Angle	23	Р	Q	75	1.0256	1.0403	1.0358
	of shine	MW	Mvar	MW	Mvar	(P.U)	degree	24	Р	Q	75	1.0620	1.0589	1.0750
1	Slack	518.84	10.4	0	0	1.030	0	25	Р	Q	75	1.0581	1.0429	1.0430
2	PV	326.81	4.848	80	12.7	1.031	-4.9924	26	Р	Q	75	1.0621	1.0750	1.0556
3	PV	402.54 592.05	2.739	90	1.9	1.00	-12.758	27	Р	Q	75 75	1.0332	1.0115	1.0098
5	F V DV	145.26	5 229	90	8.2	1.00	-13 229	28	P	Q O	75	1.0012	1.0150	1.0356
6	PV	119.85	1.018	50	2.2	1.01	-8.561	29	P	Q O	75	1.0249	1.0300	1.0338
7	PV	310.04	3.21	110	3.8	1.04	-11.542	30	P	۹ ٥	75	1.0562	1.0102	1 486
8	PV	60.248	1.005	90	1.5	1.01	-13.132	32	P	Q	75	1.0251	1.0220	1.0112
9	PV	56.023	0.95	70	1.3	1.04	-7.054	33	P	0	75	1.0419	1.0623	1.0426
10	PV	21.636	0.025	15	0.7	1.06	-13.256			~				
11	PQ			60	4.7	1.0185	-10.227				T	ABLE IV		
12	PQ			110	15	1.0504	-13.229		ACTIVE .	AND REA	CTIVE POW	ERS OF GENERAT	FORS AT 75%	LOAD
13	PQ			70	5.7	1.0186	-8.7519			T17	T29	T48	T49	T56
14	PQ			80	10.6	1.0401	-14.811		Value	0.986	0.965	0.932	0.969	0.978
15	PQ			85	3.8	1.0325	-15.025		LP	0.968	0.949	0.9821	0.9752	0.9861
16	PQ			56	4.8	1.0502	-14.84		ANN	0.941	0.956	6 0.9784	0.981	0.9932
1/	PQ			60	4.6	1.0517	-15.269							
18	PQ			55 95	5.8	1.0429	-15.301				Т	ABLE V		
19	PQ			65 50	9 14	1.0270	-10.05			SI	HINES VOLT	fages at 15% lo	DAD	
20	PQ			140	14	1.0201	-12.301	Shine	Kind	ness l	Load li	nitial voltage	Final	Final
21	PO			50	15	1.0541	-11 256		of sh	nine			voltage	voltage
23	PQ			100	29	1.0242	-9.659						(LP)	(ANN)
24	PQ			80	11	1.0541	-15.236	1		Slack		1.030	1.0705	1.0826
25	PQ			70	24	1.0579	-16.235	2		PV	115	1.025	1.0429	1.0644
26	PQ			105	10	1.0600	-12.326	3		PV	115	0.95	1.0248	1.0337
27	PQ			80	21	1.0305	-16.230	4		PV	115	1.01	1.0578	1.057
28	PQ			70	15	0.9850	-12.123	5		PV	115	1.03	1.0527	1.069
29	PQ			86	4.2	1.0159	-11.325	6		PV	115	0.94	1.0025	1.0102
30	PQ			120	9.2	0.9895	-17.0	7		PV	115	1.00	1.0029	1.0031
31	PQ			170	38	1.0500	-14.231	8		PV	115	1.01	1.0059	1.0090
32	PQ			65	10.2	1.0179	-16.025	9		PV	115	1.01	1.0520	1.0430
33	PQ			152	36	1.0362	-18.369	10		PV	115	1 02	1 0471	1 0382
			TADI	с н				11		PO	115	0.9900	1 0282	1 0314
		INTELAL '		E II DANGEC	DMEDC			12		PO	115	1 0201	1.0202	1 0202
Transf		INITIAL	TAPS OF T	KANSFO	RMERS	t ive	Depative	12			115	0.0201	1.0400	1.0353
Talisi	on on one of the	Tan	T	an	reso			13			115	1.0300	1.0341	1.0354
T	P	Тар		T48		9	T17	14		PQ	115	1.0209	1.0498	1.0321
0.9	78	0.969	0.9	932	0.9	65	0.986	15		PQ	115	1.0025	1.0456	1.0278
								16		PQ	115	1.0108	1.0491	1.0382
			TABLI	ΞШ				17		PQ	115	1.0230	1.0468	1.0389
		SHINES V	VOLTAGES	S AT 759	% LOAD			18		PQ	115	1.0056	1.0433	1.0326
Shine	Kindness	Load	Initia	l voltag	ge F	inal	Final	19		PQ	115	0.9859	1.0328	1.0101
	of shine				vo	oltage	voltage	20		PQ	115	1.0200	1.0011	1.0045
						(LP)	(ANN)	21		PQ	115	1.0216	1.0102	1.0456
1	Slack			1.05	1	.0705	1.0684	22		PQ	115	1.0365	1.0625	1.0426
2	PV	75		1.045	1	.0429	1.0422	23		PQ	115	0.9895	1.0110	1.0210
3	PV	75		1.01	1	.0248	1.0295	24		PQ	115	1.0369	1.0528	1.0569
4	PV	75		1.07	1	.0578	1.0523	25		PQ	115	1.0319	1.0652	1.0702
5	F V PV/	75		1.03	1	0253	1.005	26		PO	115	1.0405	1.0320	1.0452
7	PV	75		1.05	1	.0456	1.0360	27		PO	115	1 0305	1 0602	1 0721
, 8	PV	75		1.01	1	.0095	1.0112	27 20		PO	115	T.0202	1 0210	1 0262
9	-	75		1.06	1	.0706	1.0685	20			115	0.3330	1.0210	1.0502
-	PV	/5					1 0906	29		rų	112	0.9850	0.9820	0.9952
10	PV PV	75		1.07	1	.0826	1.0890			DC	11-	A 0704	4 0 2 0	1 111111
10 11	PV PV PQ	75 75	1	1.07 .0196	1 1	.0826 .0282	1.0295	30		PQ	115	0.9791	1.020	1.0300
10 11 12	PV PV PQ PQ	75 75 75 75	1	1.07 .0196 .0566	1 1 1	.0826 .0282 .0486	1.0295 1.0502	30 31		PQ PQ	115 115	0.9791 1.0361	1.020 1.0426	1.0300 1.0523
10 11 12 13	PV PV PQ PQ PQ	75 75 75 75 75	1 1 1	1.07 .0196 .0566 .0228	1 1 1 1	.0826 .0282 .0486 .0341	1.0295 1.0502 1.0336	30 31 32		PQ PQ PQ	115 115 115	0.9791 1.0361 1.0015	1.020 1.0426 1.0112	1.0300 1.0523 1.0210
10 11 12 13 14	PV PV PQ PQ PQ PQ	75 75 75 75 75 75	1 1 1 1	1.07 .0196 .0566 .0228 .0438	1 1 1 1	.0826 .0282 .0486 .0341 .0598	1.0295 1.0502 1.0336 1.0489	30 31 32 33		PQ PQ PQ PQ	115 115 115 115	0.9791 1.0361 1.0015 1.0056	1.020 1.0426 1.0112 1.0230	1.0300 1.0523 1.0210 1.0321
10 11 12 13 14 15	PV PV PQ PQ PQ PQ	75 75 75 75 75 75 75	1 1 1 1 1	1.07 .0196 .0566 .0228 .0438 .0428	1 1 1 1 1	.0826 .0282 .0486 .0341 .0598 .0456	1.0295 1.0502 1.0336 1.0489 1.0439	30 31 32 33		PQ PQ PQ PQ	115 115 115 115	0.9791 1.0361 1.0015 1.0056	1.020 1.0426 1.0112 1.0230	1.0300 1.0523 1.0210 1.0321
10 11 12 13 14 15 16	PV PV PQ PQ PQ PQ PQ	75 75 75 75 75 75 75 75	1 1 1 1 1 1	1.07 .0196 .0566 .0228 .0438 .0438 .0428	1 1 1 1 1 1 1	.0826 .0282 .0486 .0341 .0598 .0456 .0491	1.0295 1.0502 1.0336 1.0489 1.0439 1.0455	30 31 32 33		PQ PQ PQ PQ	115 115 115 115	0.9791 1.0361 1.0015 1.0056	1.020 1.0426 1.0112 1.0230	1.0300 1.0523 1.0210 1.0321
10 11 12 13 14 15 16 17	PV PQ PQ PQ PQ PQ PQ PQ	75 75 75 75 75 75 75 75 75	1 1 1 1 1 1 1	1.07 .0196 .0566 .0228 .0438 .0428 .0428 .0536 .0577	1 1 1 1 1 1 1 1	.0826 .0282 .0486 .0341 .0598 .0456 .0491 .0468	1.0295 1.0502 1.0336 1.0489 1.0439 1.0455 1.0416	30 31 32 33		PQ PQ PQ PQ	115 115 115 115	0.9791 1.0361 1.0015 1.0056	1.020 1.0426 1.0112 1.0230	1.0300 1.0523 1.0210 1.0321
10 11 12 13 14 15 16 17 18	PV PQ PQ PQ PQ PQ PQ PQ PQ	75 75 75 75 75 75 75 75 75 75	1 1 1 1 1 1 1 1	1.07 .0196 .0566 .0228 .0438 .0428 .0536 .0577 .0529	1 1 1 1 1 1 1 1 1	.0826 .0282 .0486 .0341 .0598 .0456 .0491 .0468 .0433 .0433	1.0295 1.0502 1.0336 1.0489 1.0439 1.0455 1.0416 1.0384	30 31 32 33		PQ PQ PQ PQ	115 115 115 115	0.9791 1.0361 1.0015 1.0056	1.020 1.0426 1.0112 1.0230	1.0300 1.0523 1.0210 1.0321
10 11 12 13 14 15 16 17 18 19 20	PV PQ PQ PQ PQ PQ PQ PQ PQ PQ PQ	75 75 75 75 75 75 75 75 75 75	1 1 1 1 1 1 1 1 1	1.07 .0196 .0566 .0228 .0438 .0428 .0536 .0577 .0529 .0336 .0262	1 1 1 1 1 1 1 1 1	.0826 .0282 .0486 .0341 .0598 .0456 .0491 .0468 .0433 .0328 .0328	1.0896 1.0295 1.0502 1.0336 1.0489 1.0489 1.0439 1.0455 1.0416 1.0384 1.0384	30 31 32 33		PQ PQ PQ PQ	115 115 115 115	0.9791 1.0361 1.0015 1.0056	1.020 1.0426 1.0112 1.0230	1.0300 1.0523 1.0210 1.0321

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TABLE VI TAPS OF TRANSFORMERS AT 115% LOAD T56 T49 T48 T29 T17 Value 0.978 0.969 0.932 0.965 0.986 LP 0.9861 0.9752 0.9821 0.9981 0.9885 ANN 1.0105 0.9974 0.9659 0.9865 0.9901

TABLE VII THE COMPARISON OF EXECUTION TIMES

22 DUS	LP	ANN			
33 608	17.8sec	6.51sec			

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