# Application Quality Function Deployment (QFD) Tool in Design of Aero Pumps Based on System Engineering

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**Abstract**—Quality Function Deployment (QFD) was developed in 1960 in Japan and introduced in 1983 in America and Europe. The paper presents a real application of this technique in a way that the method of applying QFD in design and production aero fuel pumps has been considered. While designing a product and in order to apply system engineering process, the first step is identification customer needs then its transition to engineering parameters. Since each change in deign after production process leads to extra human costs and also increase in products quality risk, QFD can make benefits in sale by meeting customer expectations. Since the needs identified as well, the use of QFD tool can lead to increase in communications and less deviation in design and production phases, finally it leads to produce the products with defined technical attributes.

*Keywords*—Customer voice, engineering parameters, QFD, gear pump.

#### I. INTRODUCTION

THE goal of the paper is applying QFD tool in aero pump design. Since each product can be defined as a system, so the use of special tools in system engineering process causes that needs would be met. QFD was formed based on total quality control, it means that the control would be applied not only in production lines but also the needs should be considered before design phase. for the first time After World War II the Japanese companies focused on design quality [1], although before that the need to understand the design requirements was sensed but no normal system existed in order to transform customer needs to initial design [2], consequently QFD established as a design correction method for meeting customer needs. Design teams in suitable design of a product need to know what thing to be designed and also expectations of end users. QFD is a systematic method based on exact identification of customer needs and related to functional groups in companies; it means that by applying QFD the customer needs would be translated to design parameters and the details determined in product development.

#### II. EXPRESS AND DEVELOPMENT OF QFD

#### A. General

QFD is a tool that customer requirements are identified in design phase, this process done by different methods including: brain storming, compliments search, Warranty logs,

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customer visitation and concentrated groups. Akao was named as father of QFD. He defined "the method for design quality development which helps to customer satisfaction and customer requirements and transition to considered goals in desired design and quality, then it being used in production phases [3].

#### B. QFD Structure

The first stage of applying QFD is providing House Of Quality. The House is graphic tool in order to define the relationships between customer needs to product. Fig. 1 shows HOQ format:



Fig. 1 HOQ Matrix [4]

#### C. Customer Needs

Firstly customer needs or WHATS are identified that may be stated as general and vague. The Japanese have called this stage "voice of customer"; these needs are expressed in different levels as primary, secondary, tertiary.

#### **D.**Engineering Attributes

Then engineering attributes or How's are selected based on customer needs and also should be measurable in a way that customer needs would be satisfied.

# *E. The Relationship between Customer Needs and Engineering Attributes*

After putting Whats and Hows in house of quality, now the relationship between them is set by using symbols shown as:

- Strong relationship
- Medium relationship
- Weak relationship

# F. Customer Rating of the Competition

It expresses that how new product competes with other available products; this aspect of product is vital for competition and get new product. Acceptable competitive comparison information would be acquired by engineers and taking note of what customers says at trade shows and retail outlets. The rate which representing the competition for each requirements are given from 0 to 5.

#### G. Correlation Matrix

The designers in design process have challenges because of no information about the impact of each design parameters on other parameters and how these factors can be effective on customer needs. The relationships among them in QFD's roof guide product designer. In relative and absolute importance part, total of scores is brought at bottom of chart, it states that how much customer needs are met.

### H.QFD Advantages

This technique enables organizations to be more competitive in design, have better quality and less cost furthermore it helps to develop new product.

Decrease engineering's changes

- Decrease set up changes
- Meet customer requirements
- It is proactive instead of reactive

Fig. 2 shows the whole process of QFD, as it is considered that another advantage of which is transition the available knowledge among different stages and be sure of tracing the requirements in a way that all requirements would be met and also final product toward main needs is traceable.

#### III. APPLICATION QFD

In the paper application QFD for aero pumps has been done according to Fig. 2, since the considered pump is prototype so, 3 and 4 stages have been merged. Pump is a tool which gets the required mechanical energy from external power like electromotor and affects passing fluid consequently; so energy of fluid is increased in pump outlet and it leads to pressure and flow. A pump should make the required flow as continuous and stable besides generate the considered pressure or Head in all stages of pump working. Therefore, a designer should consider these conditions while designing a pump in order to meet all user needs.



Fig. 2 Overall QFD Transfer Process [5]

Gear pumps combined by two or some gears which one is driver and others are driven, the entered force to pump by driver gear transfers to driven one. The gear of a pump is same as pump's heart; its most important function is transition of fluid. Aero pumps are considered as products with narrow markets so, customers have enough technical knowledge about their requirements. In order to reduce the risk here customer requirements and technical requirements have lots in common. Therefore, it is important to define precisely customer requirements. According to recent researches, customer technical requirements for considered pump as Fig. 5 in phase 1 QFD. The needs are defined as primary one then secondary or even more divisions.

In continuous impact of technical parameters of pump and organizational difficulty are put on chart besides relationship between parameters in chart's roof as Fig. 6. Then in right part of chart, the considered pumps in comparison with competitors are shown in Fig. 7. In addition, the phase 1, QFD chart is shown in Fig. 8.

To proceed should formed phase 2 and 3 QFD charts. The phase 2, design parameters, and QFD chart are shown in Figs. 9 and 10. In addition, the phase 3, design parameters in manufacturing and QFD chart are shown in Figs. 11 and 12.



Fig. 3 Gear pump operation



Fig. 5 Customer re	equirements
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low lubricity, resistance to deterioration, 100 hours, (ARP 1797)

primary fuel: MIL-T-5624, Grade JP4

humidity resistance- 95% or higher humidity

maximume and minimume fue inlet pressure, 8-50 psia

minimume & maximume temprature (-54°C to 90°)

accelerated aging, minimum temp. 71°C, minimume 168 hours

alternate fuel

vibration-MIL- STD- 810

fuel type

enviroment

condition

regulation

5

3

4

4

3

4

3

4



#### Fig. 6 Quality house's roof

		How			custo	mer i	rating	ş
Whats	(REQUIRE	MENT)	mportance	worse	A B	pump pump	Δ	better
primary	secondary	tertiary		1	2	3	4	1 3
		min fuel flow @ max. speed and max pressure	5					14
	Dunn	min fuel flow @ max. speed and min pressure	4					1
performance	Characteristic	min fuel flow @ idlle speed and max pressure	4					
	Characteristic	min fuel flow @ idlle speed and min pressure	4	1		1		
performance		min fuel flow @ min. speed and max pressure	5					
	max torque		4				4	
	max power		3	-			4	
	rotation directi	on-CCW	4				-	Pa
	length		3	i		4		
physical	width		3	2		4		
characteristic	height		3			4		
	dry weight		3			0	-	
	mean time to p	epair	3					
maintenance	total maintenan	ace man houre	3					し
	initial costs, pu services)	urchase price (pump, system, pipe, auxiliary	4				6	1
life cycle	installation and	d commissioning cost (including training)	3		-	6		T
	operation costs	(labor cost of normal system supervision)	4				0	Þ
	maintenance an	nd repair costs (routine and predicted repairs)	4				6	Г
cost	down time cos	ts(loss of production)	3				1	Г
	enviromental c auxiliary equi	osts(contamination from pumped liquid and pment)	4					
	decommission local environm	ing/disposal costs (including restoration of the tent and disposal of auxiliary services).	2					N
raliability	mean time bety	ween removals	5	1				1
renability	mean time betw	ween failure(MTBF)	5	÷				
î	endurance	100 hours or 600 cycle at high temp.(+120° C)	4					1
	characteristic	300 hours or 1800 cycle at room temprature	4					1
	enaracteristic	20 hours or 120 cycle at low temprature(-54 °C)	3					1
	fire resistance	at 1090 °C for 5 minutes	5				_	1
	fuel pump capa engine perform	able of operated for 5 hours at design maximume nance at 30,000 feet,	4					4
regulation	fuel pump cavi maximume req	itation, 47 hours at intermediate rated speed and uiered flow and pressure(ARP 492)	5					4
	low lubricity .	resistance to deterioration, 100 hours, (ARP 1797)	5					1
	accelerated agi	ng, nunimum temp. 71°C, minimume 168 hours	3	_	-		_	14
	vibration-MIL	- STD- 810	4		-			1
	fuel type	primary fuel: MIL-T-5624, Grade JP4	4	-	-	_	_	14
		alternate fuel	3		-	-	-	4
	enviroment	numidity resistance- 95% or higher humidity	4	-	-	_	_	14
	condition	maximume and minimume rue inter press.8-50 psia	5	_	-	-	_	14

Fig. 7 Technical competitive comparison

	impo		Boost		IIIKI	film			gear pump			valve	relief	vib	rotation		
Whats	(REQUIRE	MENT)	ortance	flow rate	pressure rate	efficiency	filter O.D. pressure	max press. drop	flow rate	pressure rate	efficiency	force on gear shaft	force on bearing	cracking pressure	fully open flow	ration	direction
		_					_										
primary	secondary	tertiary		0		-			0		-				-		-
		min fuel flow @ max. speed and max pressure	2	Θ	0	0			Θ	Θ	0	<u> </u>	<u> </u>	0	Θ		-
	Pump	min fuel flow @ max. speed and min pressure	4	Θ	Θ	0	<u> </u>		Θ	Θ	Θ	<u> </u>	<u> </u>	0	•		
	Characteristic	min fuel flow (a) idlle speed and max pressure	4	Θ	Θ	0	-	-	0	Θ	Θ	<u> </u>	<u> </u>				
performance		min fuel flow @ idlle speed and min pressure	4	Θ	0	0	-		0	Θ	Θ			<b>A</b>			
1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1		min fuel flow (a) min. speed and max pressure	2	Θ	Θ	0	-	<b>A</b>	Θ	Θ	Θ		-	•			
	max torque		4		0	•	-	-		<b>A</b>	-	Θ	0				<u> </u>
8	max power	0000	3	•	0	•	-		Θ	Θ	0	0	-				
	rotation directi	on-CCW	4		-	-	<u> </u>				-	<u> </u>	<u> </u>	-			Θ
	length		3	•		-			•	•		<u> </u>	-				<u> </u>
physical	width		3	•		-				•							
characteristic	height		3	•						•							
L	dry weight		3				-		<b>A</b>								<u> </u>
maintenance	mean time to r	3		•	•	<u> </u>	•		-	•	<b>A</b>	•	•			—	
	3		-	-	-		-	-		<b></b>	•				-		
	services)	irchase price (pump, system, pipe, auxiliary	4	•	0	Θ	0	•	0	0	Θ	•	0	0	0	Θ	•
	installation and	d commissioning cost (including training)	3		•	0		•									
	operation costs (labor cost of normal system supervision)										0						
life cycle	maintenance an	nd repair costs (routine and predicted repairs)	4		0	0	•	•			0	0	0	•		0	
cost	down time cos	3								•							
3	enviromental costs(contamiration from pumped liquid and auxiliary equipment)					0					•						
	decommission	ing/disposal costs (including restoration of the	2									0	0				
- 000000	mean time bet	veen removals	5			0	0	0		-		0		0		Θ	
reliability	mean time bet	veen failure(MTBE)	5		-	0	0	0	-		-	0	-	0		0	
	incuir tine oct	100 hours or 600 cycle at high term (+120° C)	4		0	0	- ×	-	Θ	Θ	Θ		-			0	
	endurance	300 hours or 1800 cycle at room temprature	4	-		0	-	-	Θ	Θ	0	-	-	-	-	0	
	characteristic	20 hours or 120 cycle at low temprature(-54 °C)	3		0	0			Θ	Θ	Θ					0	
	fire resistance	at 1090 °C for 5 minutes	5			0											
	fuel pump capa	able of operated for 5 hours at design maximume			0	0			0	0							
2	engine perform	nance at 30,000 feet,	*	•	0					0					. <b>.</b>		
	fuel pump cavi maximume req	tation, 47 hours at intermediate rated speed and miered flow and pressure (ARP 492)	5			0		•	0	0		0	0			0	
regulation	low lubricity	resistance to deterioration 100 hours (ARP 1797)	5	0		0					Θ	0	0			A	
	accelerated agi	ng, minimum temp, 71°C, minimume 168 hours	3	Ă		Å			-		-	-		Ā			
	vibration-MIL-	STD- 810	4									Θ		0		0	
2	Gultur	primary fuel: MIL-T-5624, Grade JP4	4														
	fuel type alternate fuel humidity resistance- 95% or higher humi		3														
9			4											š			
	condition	maximume and minimume fue inlet press.8-50 psia	3		0		Θ			0	0		1	•			
minimume & maximume temp. (-54°C to 90°)																	
	or		5	6	7	4	4	7	8	9	8	8	7	8	8	2	
		absolute importance		276	338	379	98	64	399	403	427	177	103	183	92	214	43

# Fig. 8 Phase 1 of QFD chart

	Part Design Parameters			propertice	impeller										main pump											propertice	filter			propertice	-
	(HOW)	customer t	importa	tip clearanc	imj							propertice	gear					diffre	inl		propertice		inlet ar	lu dund	filter s	spri	elemen	elem	relief valv	sealing s	valv
	Design requirement	argets	nce	ce impeller/housing	peller angle	pitch	width	teeth number	pressure angle	pitch diameter	root diameter	clearance gears(ξ)	gear core hardness	gear case hardness	tip clearance gear/body	geometry total runout	tooth profile tolerance	ntial pressure	et pressure	bearing O.D.	bearing I.D.	surface roughness	ea	pm	spring siffness	ng seat area	t mesh number	ent mesh size	ve spring stiffness	urface roughness	e cross area
Γ	design difficulty	6		8	6	5	4	1	4	6	6	7	9		8			5	5	6	6	6	3	3	5	5	5	5	5	8	5
	parameter values			0.008-0.015 in	(-) Degree	(-) 1/in	(-) in	•	20 degree	(-)in	(-) in	(-)	(-) HRC	(-) HRC	(-) in	(-) in	(-) in	(-) psid	(-) psig	(-) in	(-) in	(-) µ.in	(-) squre.in	(-) rpm	(-) Ib/in	(-) squre.in	(-)	(-) in	(-) Ib/in	(-) µ.in	(-) squre.in

Fig. 9 Design parameters of phase 2



Fig. 10 Phase 2 of QFD chart

Manufacture Design Parameter	Milling	CNC			Gear Manufacture					parameter	Spring		1 uning	Turning
(HOW)	SIVUC	5 4410		Parameters	Hob		case deptl	spring mate	residual s		Process Parameter	11	Cu	Fee
Part Design requirement	Cutting Speed	Feeding Speed	Special class tolerance	axial feeding(in/wrev)	Radial feeding( in)	cutting speed(in/min)	h hardening (µ.in)	erial type and grade	tress in the spring	clamping stress	clamping temprature	clamping time	tting Speed	ding Speed
difficulty	8	6	9	7	8	8	9	7	6	8	6	5	6	6
parameter values	NA	NA	µ.in	in/wrev	'n	in/min	µ.in	NA	NA	NA	NA	NA	NA	NA

Fig. 11 Design parameters in manufacturing (phase 3)

# IV. ANALYSIS

In QFD table-phase 3, the parameter "special class tolerance" that used in hob machinery, has most important percentage (14.7%).

The manufacture design parameter has impact on part design requirement with equal importance coefficient as:

- Clearance gears ( $\xi$ ): importance factor=5x9=45
- Tip clearance gear /body: importance factor=5x9=45
- Geometry total run out: importance factor=5x9=45
- Tooth profile tolerance: importance factor=5x9=45

All four part design requirements belong to design

requirements of pump wheel gear since the impact of each mentioned points on customer needs in phase 1 is widespread so, one point with simple analysis is selected for analysis.

Refer to phase 2 of QFD absolute importance of four part design requirements mentioned in previous stage shows that two parameters clearance gear and tip clearance gear /body have most absolute importance equal to 113. These two parameters effect different design requirements that most important of them are brought in Table I, regarding amount of impressionable.

As a result, vibration and main gear pump -flow rate have most effective. Refer to phase 1 QFD amount of effectiveness

of mentioned parameters on customer needs shows that flow rate has absolute importance 399 and vibration has absolute importance 214. Consequently, tip clearance of gear/body has most effectiveness on engineering parameters in phase 1 QFD. Now it is stated the impact of parameter special class tolerance of phase 3 QFD on main gear pump – flow rate of phase 1 QFD and also customer requirements. Before that, a definition of hob tool is expressed.

# A. Hob

Hob is a tool that often used for produce gear profile. The production of gear is done with continues index process by rotating piece and hob together with a fixed ratio and at the same time, the hob being driven into pieces [6].

Hob tooth creates progressively and each tooth is in a different position. Hobs are made in 5 different classes. 3 classes have profile grinding and 2 classes do not have profile grinding [7].

Hob that has profile grinding:

- AA: very high accuracy
- A: high accuracy
- B: standard
- Hob that does not have profile grinding:
- C: high accuracy
- D: standard

		Manufacture Design Parameter			Milling	CNC			Gear Manufacture					parameter	Conting		Sumn	Transferre
		customer ta	importan	SIXN C	5 Avia		Parameters	Hob		case depth	spring mate	residual st		Process Parameter		Cut	Fee	
P	art Design equirement		rgets	ce	Cutting Speed	Feeding Speed	Special class tolerance	axial feeding(in/wrev)	Radial feeding( in)	cutting speed(in/min)	1 hardening (µ.in)	rial type and grade	ress in the spring	clamping stress	clamping temprature	clamping time	ting Speed	ding Speed
primary	secondary	tertiary																
impeller	tip cleara	nce impeller/housing	0.008-0.015	5	Θ	Θ												
propertice	iı	mpeller angle	(-) Degree	5	Θ	Θ												
		pitch	(-) 1/in	4														$\square$
		teeth number	(-)	4					1		(							$\square$
		pressure angle	20 degree	5						0								
		pitch diameter	(-)in	4			0											
	gear	root diameter	(-) in	3				0	0									
main	propertice	clearance gears(ξ)	(-)	5			Θ	Θ	0	0								
main		gear case hardness	(-) lb	4							Θ						_	
pump		tip clearance gear/body	(-) in	5			Θ	Θ		0								
		geometry total runout	(-) in	5			Θ	Θ	0	0								
		tooth profile tolerance	(-) in	5			Θ	Θ	Θ	0								
	hoaring	bearing O.D.	(-) in	3														
	propertice	bearing I.D.	(-) in	3	ļ.,													
	propertice	surface roughness	(-) µ.in	5			2										Θ	Θ
filter propertice	filte	r spring siffness	(-) lb/in	4								Θ	Θ	Θ	Θ	Θ		
and in family of	relief va	alve spring stiffness	(-) lb/in	4								Θ	Θ	Θ	Θ	Θ		
propertice	sealing	surface roughness	(-) µ.in	5													Θ	Θ
propertice	(-) squre.in	3																
	diffi	culty			8	6	9	7	8	8	9	7	6	8	6	5	6	6
	paramete			NA	NA	µ.in	in/wrev	'n	in/min	µ.in	NA	NA	NA	NA	NA	NA	NA	
	a	bsolute importance			90	90	200	198	102	91	36	72	72	72	72	72	102	99
		absolute weight			6.6	6.6	14.6	14.5	7.5	6.652	2.6	5.3	5.3	5.3	5.263	5.3	7.5	7.2

Fig. 12 Phase 3 of QFD chart

 TABLE I

 IMPACT OF GAINED DESIGN PARAMETERS TO ENGINEERING PARAMETERS

 Tip clearance gear/body
 Clearance gear

 Main gear
 Flow rate
 Importance factor=45

 pump
 efficiency
 Importance factor=36

 vibration
 Importance factor=45

The selection of Class accuracy depends on the piece that is built by its tolerance. For example, if hob diametric pitch is 3-3.999, hob accuracy as Table II.

TABLE II HOB ACCURACY FOR DIAMETRIC PITCH 3-3.999 [7] Hob special class tolerance в AA A Hob diameter runout 2 4 6 Outside diameter runout 5 15 25 Lead variation tooth to tooth 4 4 6 Pressure angle or tooth profile 2 3 5 Tooth thickness(minus only 15 15 15

Assume that change hob tolerance class makes change outside diameter of gear about " $\alpha$ ", then tip clearance gear/body (radial clearance) is changed about " $\alpha/2$ ".

Pump capacity in equal condition depends on radial clearance between pump body and tooth head and also inclusion fluid film, if it does not fit, leakage of fluid occurs from high pressure zone to low pressure. For gear with common size, the radial clearance range is variable from 0.8  $\mu$ .in to 8  $\mu$ .in [8]. In Fig. 13, it is seen the impact of radial clearance on gear pump volumetric efficiency.



Fig. 13 The impact of radial clearance on gear pump volumetric efficiency [8]

According to Fig. 13, change of tip clearance about " $\alpha/2$ " makes efficiency change about " $\beta$ ". Because the volumetric efficiency of gear pump is related directly to pump flow rate, so flow rate varies in ratio " $\beta$ " as per (1).

$$\eta = Q_{ef} / Q_i \to Q_{ef} = \eta \times Q_i \tag{1}$$

 $Q_{ef}$ : Effective flow rate of pump;  $Q_i$ : Nominal flow rate of pump;  $\eta$ : Pump efficiency.

As observed in phase 1, QFD table, engineering parameter "main gear pump-flow rate" affects different requirements, by considering the importance of requirement the most effectiveness as:

- Min fuel flow at max. Speed and max. Pressure  $\rightarrow$  importance factor: 5x9=45
- Min fuel flow at min. Speed and max. pressure  $\rightarrow$  importance factor: 5x9=45

The point is that what to be noted most is that the gear pump internal leakage sequence of radial clearance can be occurred further at low speed. The internal leakage sequence of radial clearance to total internal leakage is minimal by increase in pump speed. Due to radial clearance, the change in effective flow rate of pump has most effectiveness on requirement "min fuel flow at min. speed and max pressure".

#### V.CONCLUSION

As shown, QFD model facilitates translation of total and vague requirements into technical measurable requirements. Consequently, the existence of such structure leads to manage complexity in systems so, QFD is a tool for transition customer needs to technical design parameters which increases customer satisfaction and also decreases of problems in initial stage of design phase. QFD in itself does not engineering's problems; it is a forum for gathering and organizing all the data related to a design. The reason of usage QFD in aero industry is its ability to integrate physically besides the integration among customer needs, design requirements, parts characteristics, process key activities, and production requirements. In recent case study which shows the QFD matrix as a powerful tool representing the relationship between customer needs and design parameter's pump. The matrix is for negotiation between requirements in a way that it decreases no certainty in product design. The traditional method of a QFD developed in mentioned research. At first stage customer needs identified so, it compliances between customer need and product's one made. Then in following step by determining technical parameters in order to meet the needs, they were entered into QFD chart. Then the relationship between the parameters set in quality house's roof. According to calculations' results that given in last chart, absolute weights are as Table III.

TABLE III											
	A	BSOLUTE WEIGHT									
Turning	Turning Feeding Speed										
Turning		Cutting Speed	7.5								
	Hot Set	Clamping Time	5.3								
	Process	Clamping Temp	5.3								
Spring Parameter	Parameter	CLAMPING stress	5.3								
Tarameter	R	5.3									
	Spring Material Type and Grade										
	С	ase depth hardening(µ.in)	2.6								
		Cutting Speed(in/min)	6.7								
Gear	Hob	Radial Feeding(in)	7.5								
Manufacture	Machine	Axial Feeding(in/wrew)	14.3								
	Parameters	Special Class Tolerance Values in	14.7								
		μ.m									
CNC Milling	5 axis	Feeding Speed	6.6								
erve winning	5 0/15	Cutting Speed(in/min)	6.6								

The calculations for technical parameters represents that the most percentage is related to special class tolerance used in machinery in 14.7; it means that the mentioned parameter has most importance regarding to customer requirements.

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